



# Soft Robotics - Robots Designed to Interact with Humans and Unknown Environments

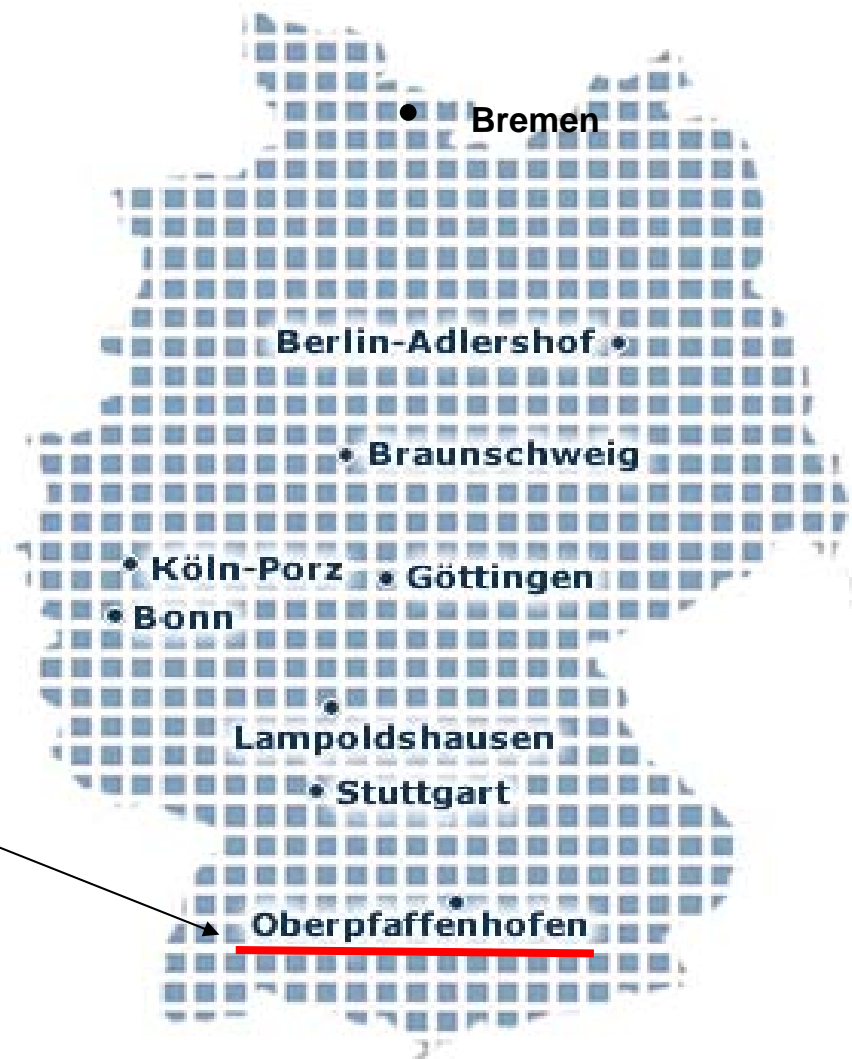
*Alin Albu-Schäffer*

*Paris, 22.01.2010*

# DLR Deutsches Zentrum für Luft- und Raumfahrt (German Aerospace Center)

- ~ 5000 employees
- nine locations

~1000 employees



research staff:~180 persons

Institute of Robotics and Mechatronics

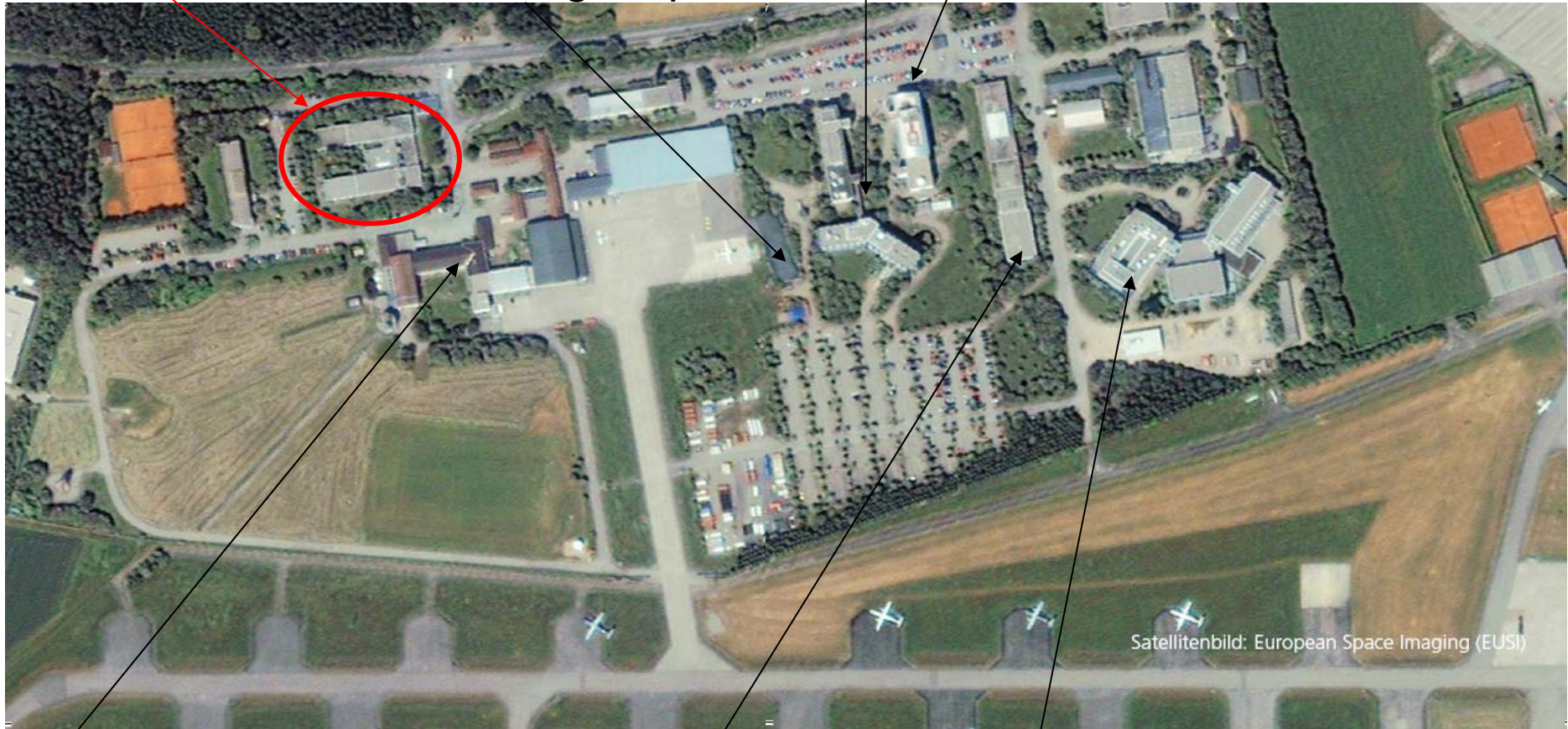
New Department "Mechatronic Systems"

76 persons

Applied Remote Sensing Cluster

Atmospheric Physics

Flight operation



Satellitenbild: European Space Imaging (EUSI)

Microwaves and radar

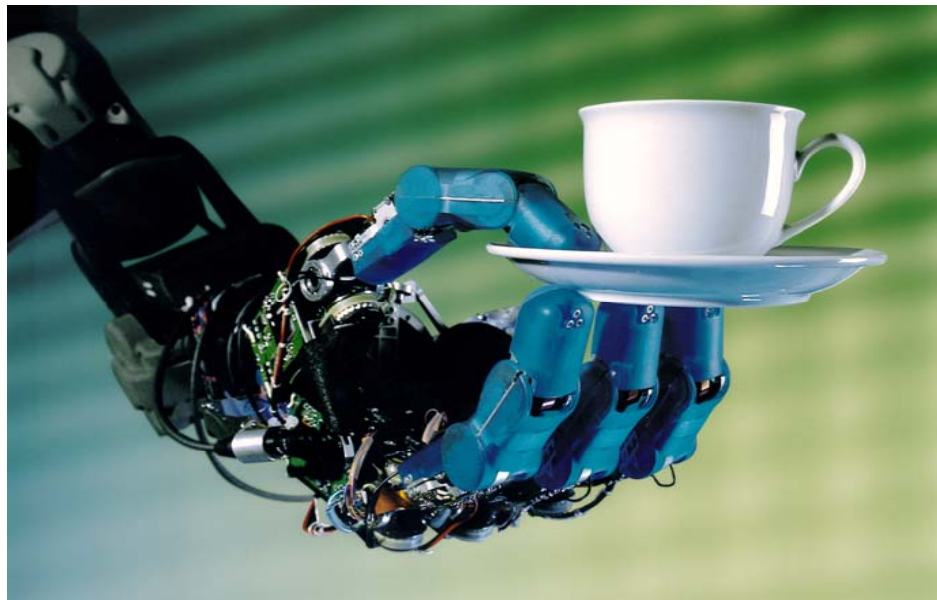
Space Operations Center  
Communications and Navigation



Deutsches Zentrum  
für Luft- und Raumfahrt e.V.  
in der Helmholtz-Gemeinschaft

# Long Experience in Development of Hand-Arm Systems

**Hand II:** 13 Joints,  
3kg finger tip force



## LBR III

load/weight ~1/1 (14kg)  
Consumed power ~150 Watt,  
Integrated Electronics

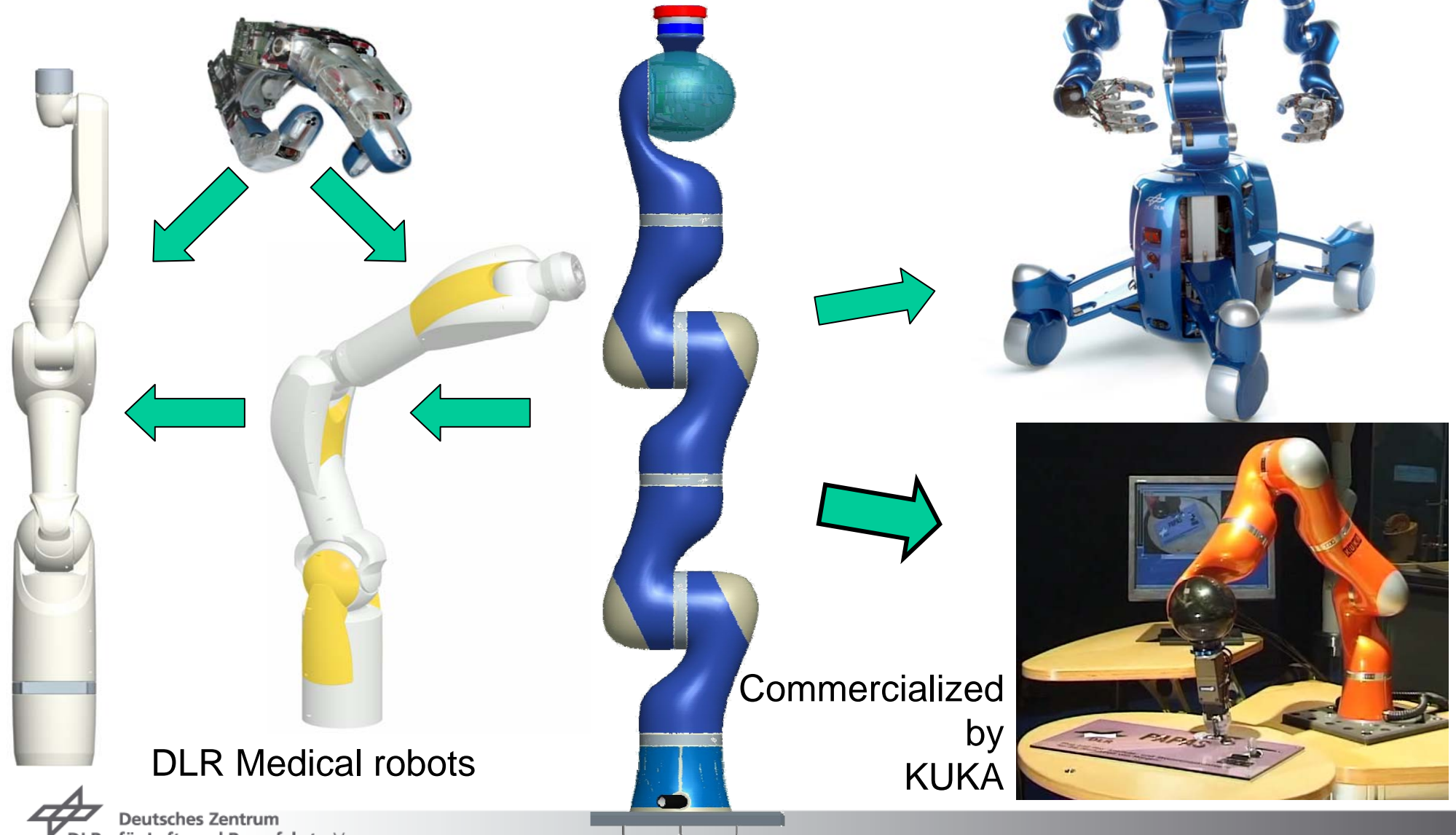


Torque Sensor



# Mechatronic Developments

Torque sensing in each joint



DLR Medical robots

Commercialized by KUKA

Justin



# Mechatronic Developments



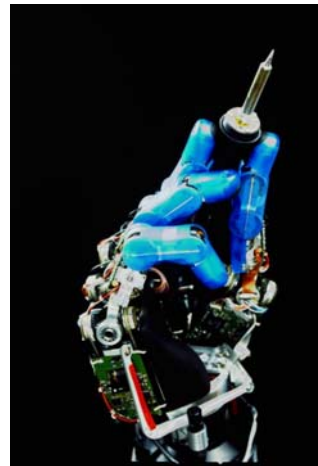
DLR-Hand IIb



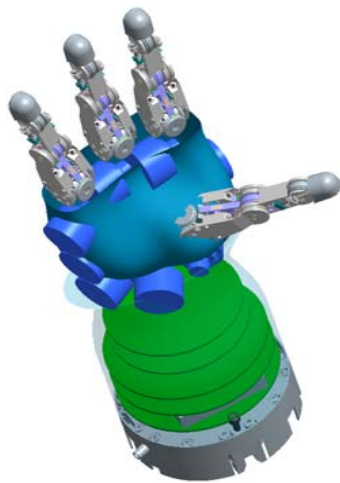
6 legged Crawler



Justin



Commercialized  
by  
Schunk



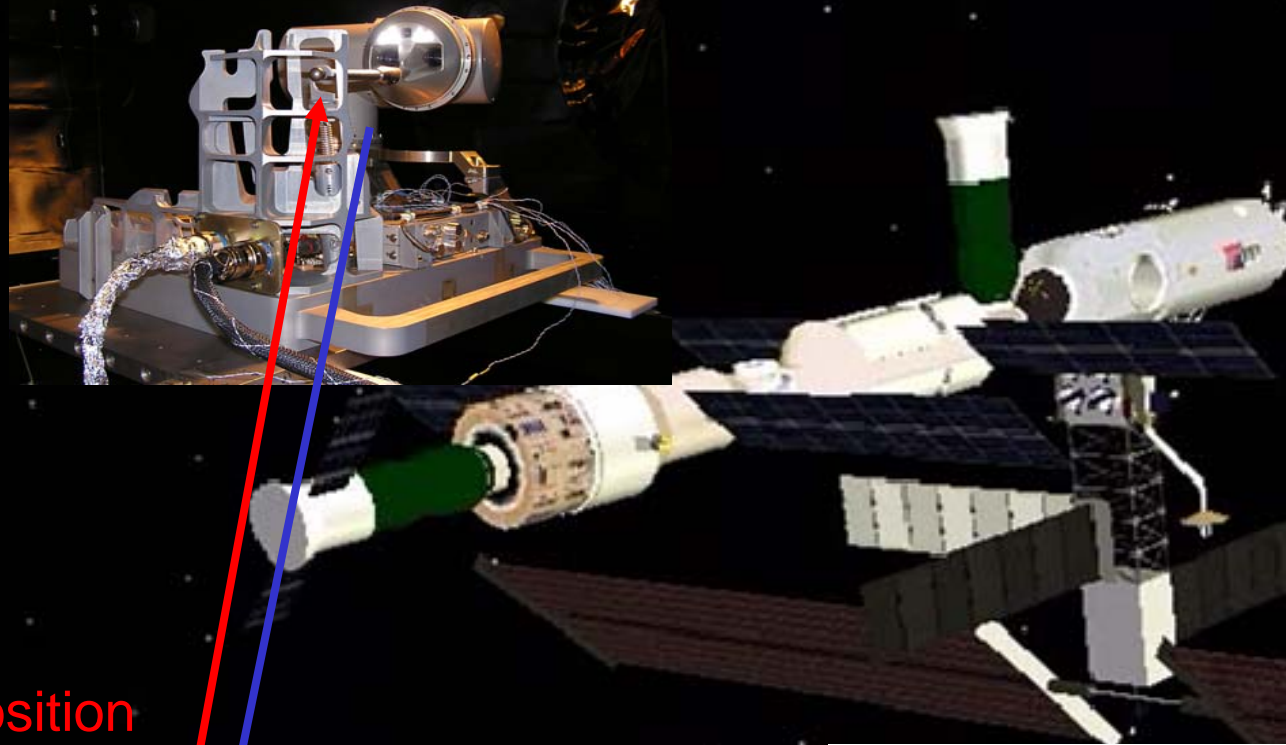
DEXHAND (ESA-Project)



DLR-HIT Hand I, II

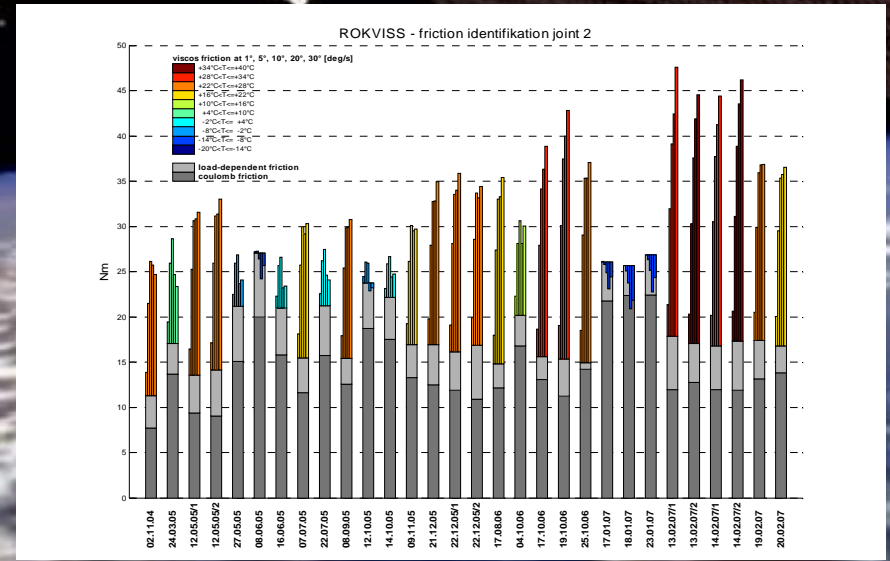
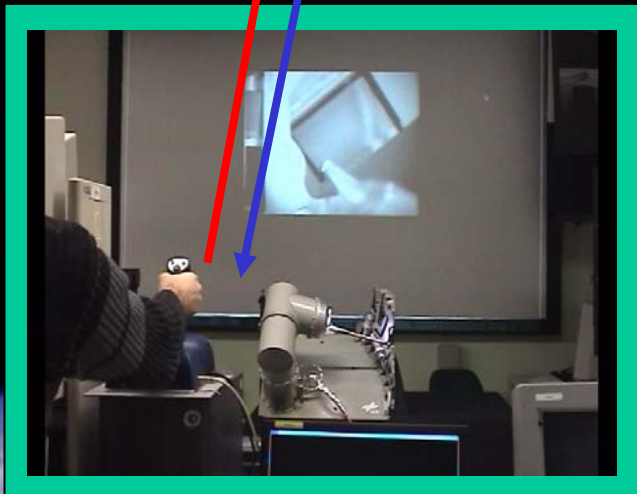


# ROKVISS



position

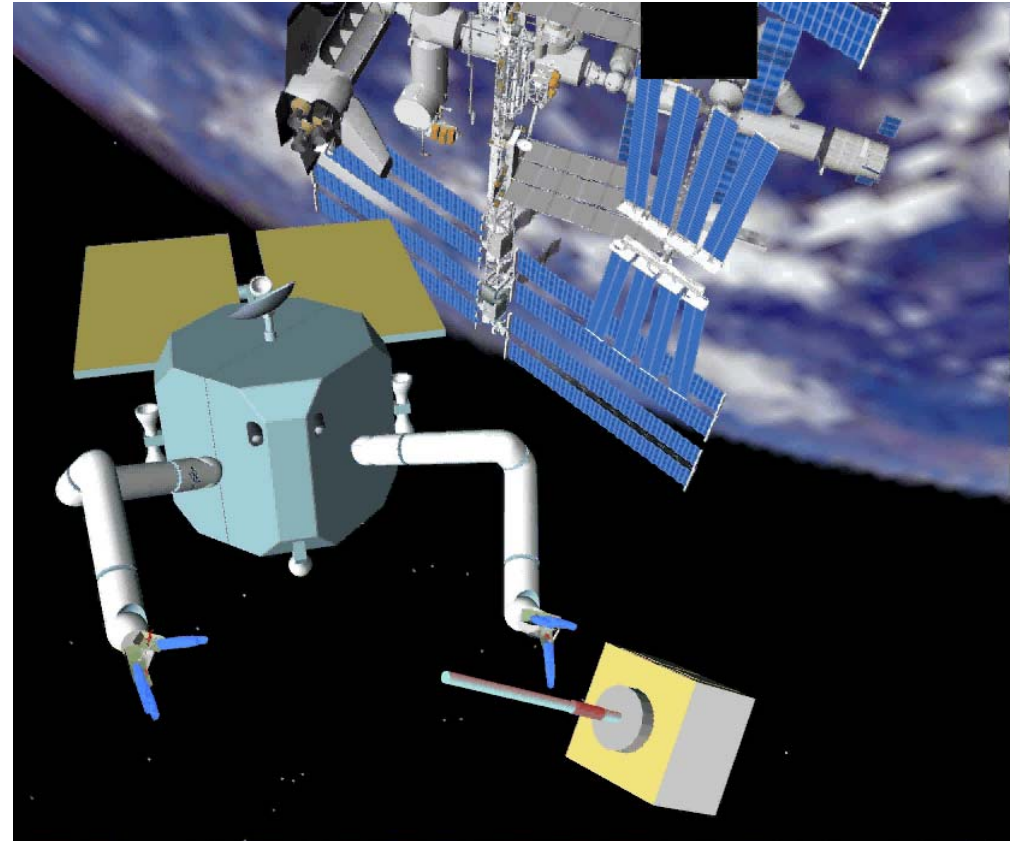
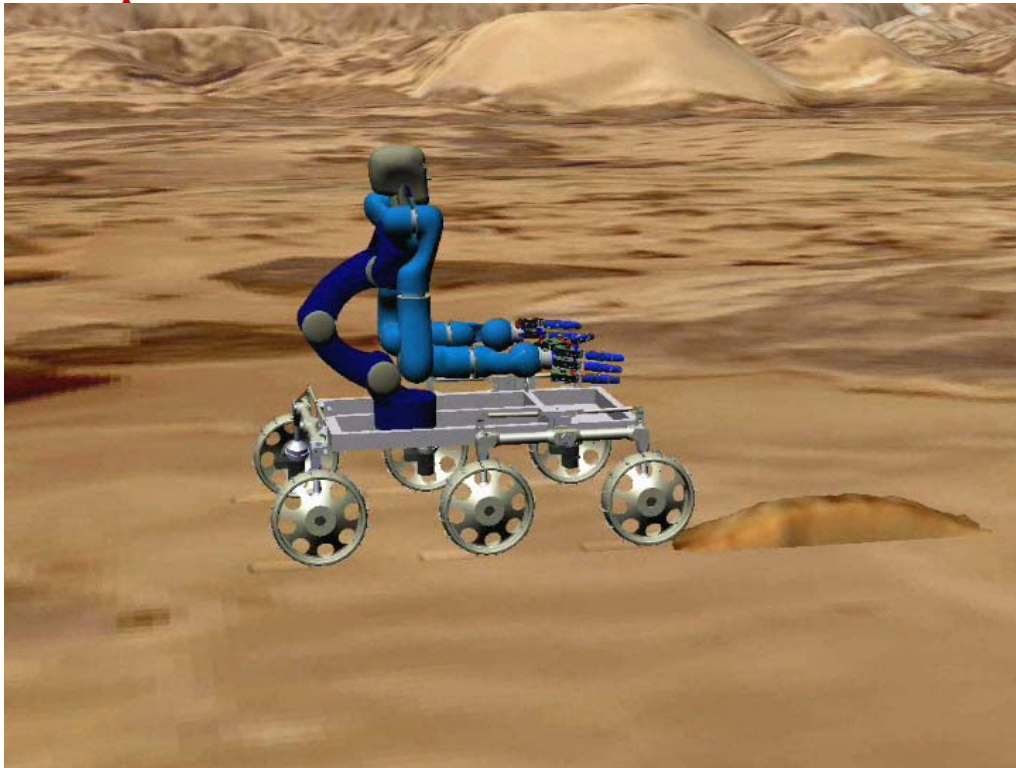
force feedback



# Space Robotics

„Affordable“, operations in space with mobile/free-flying robonauts for

- Servicing  
and
- Exploration





# Service Robotics

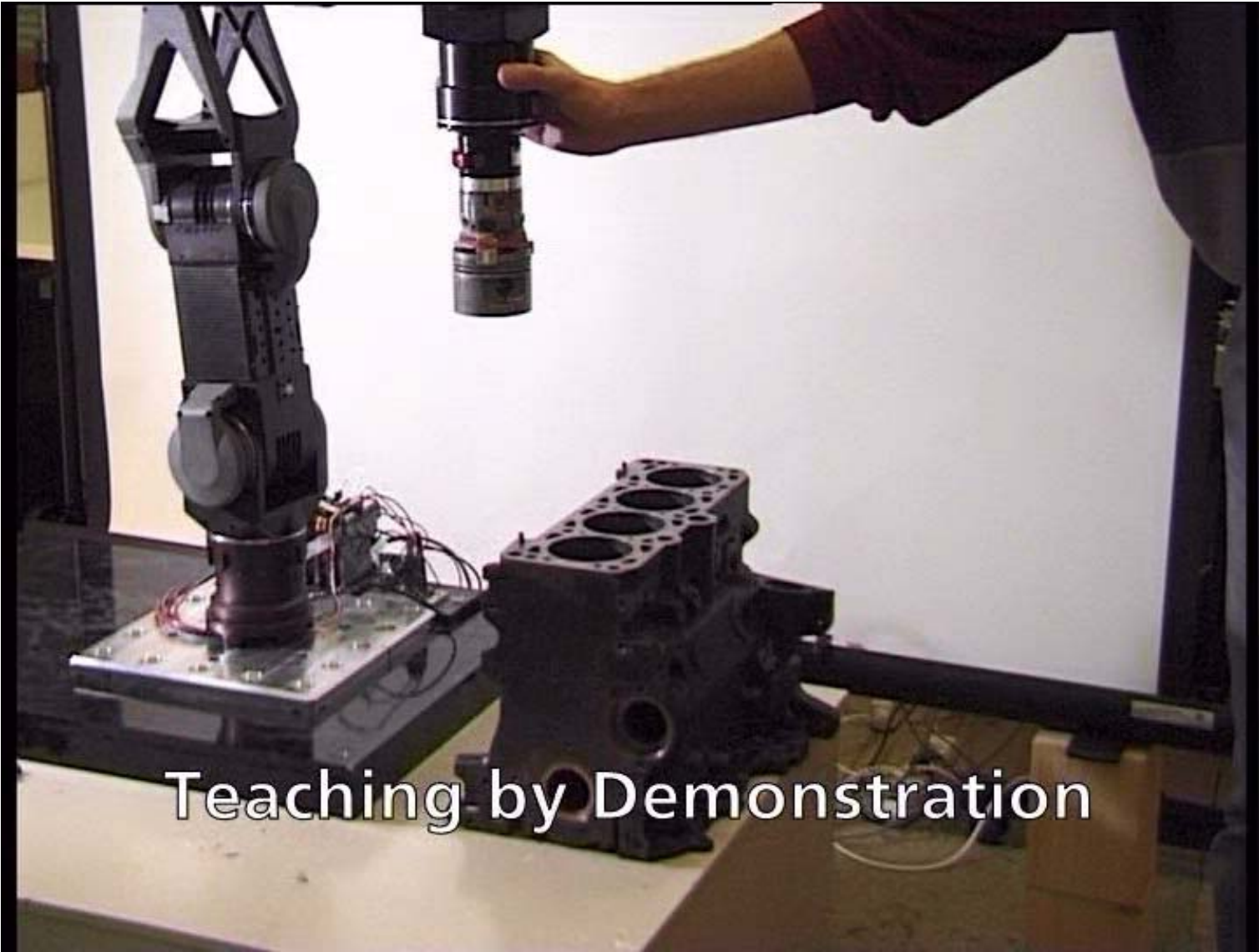


# Medical Robotics

## The MIROSURGE System



# Industrial Assistan



# Production Assistant



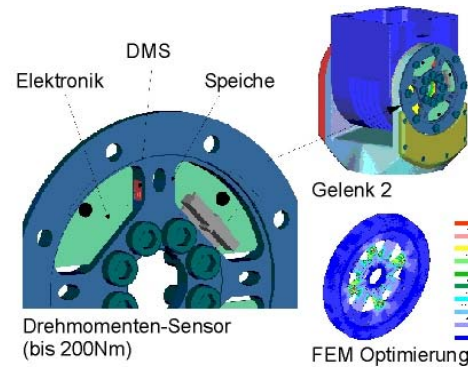
# The “mechatronic” DLR light-weight robots

**Extreme light arms with high load capabilities and integrated sensor and power electronics**

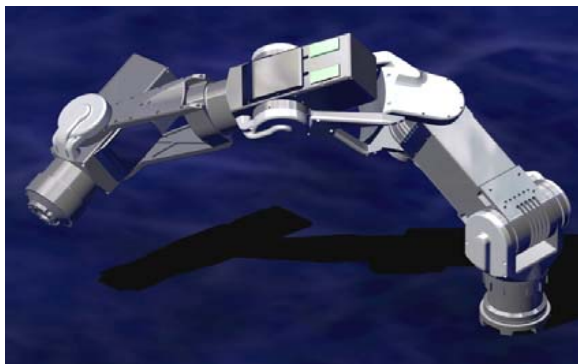
- Harmonic Drives
- motor and load side position sensors
- Joint torque sensors
- Cartesian Force-torque sensor



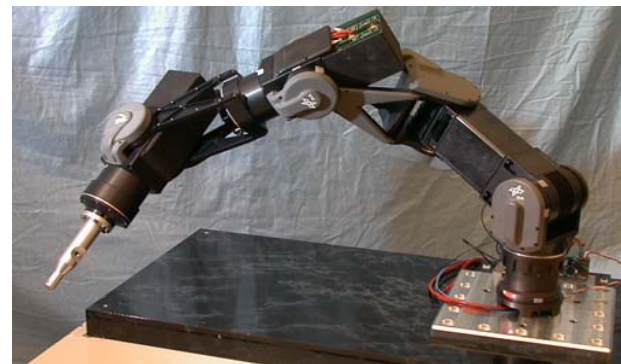
**LWR I  
(ca.1992)**



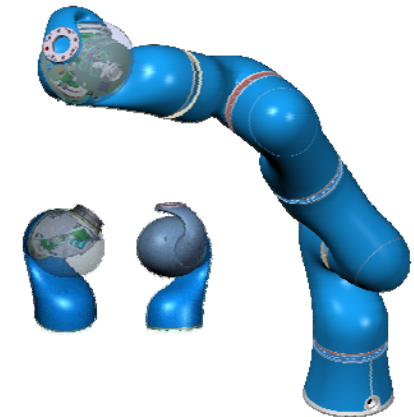
**LWR III real (2002)**



**LWR II virtual (ca.1998)**



**LWR II real (ca. 1999)**

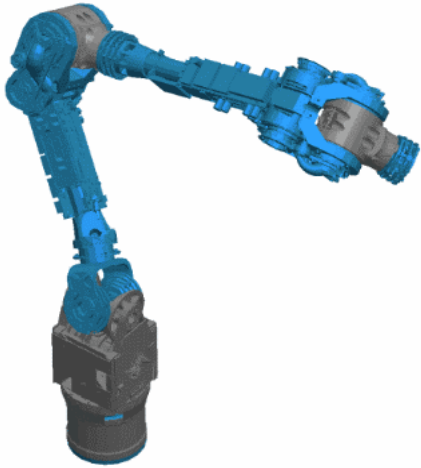


**LWR III virtual (2000)**

# Light-Weight Design

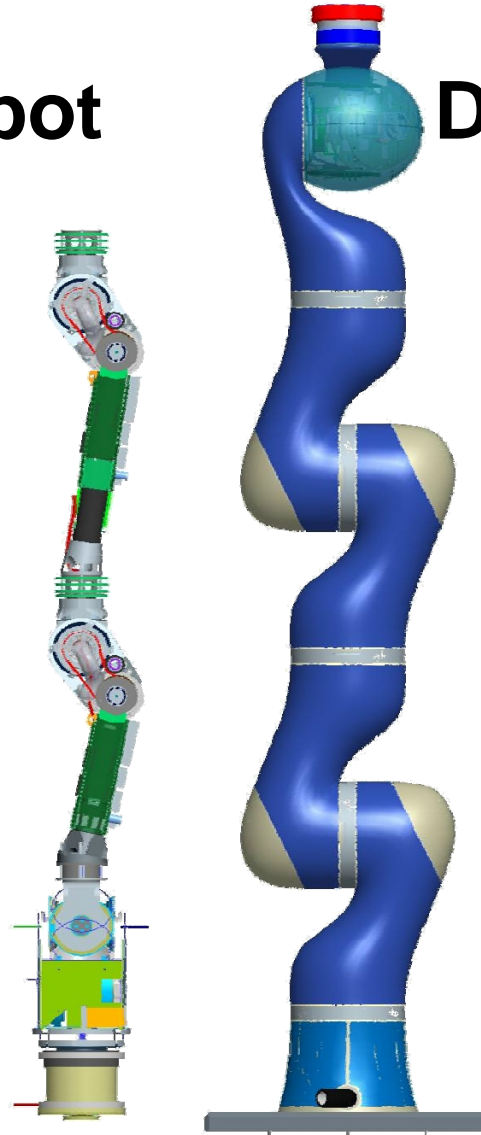
## DLR medical robot

- 7 Axes
- Weight < 10 kg
- Payload: 3 kg

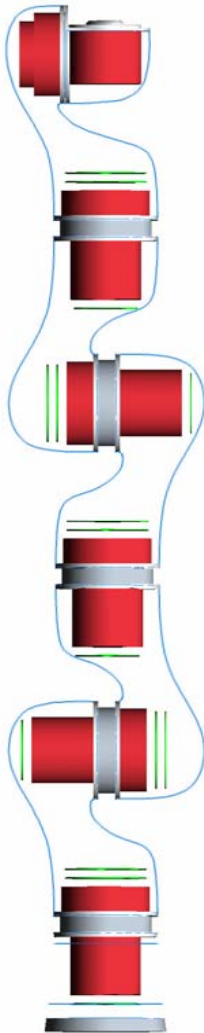
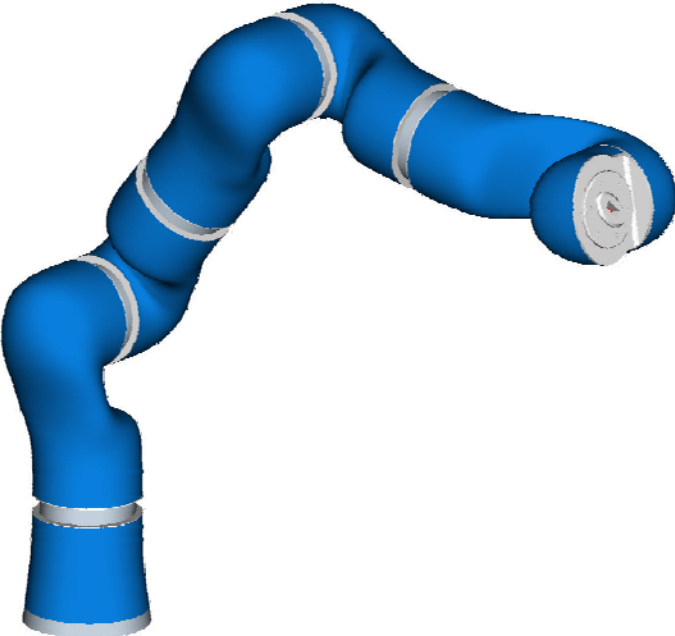


## DLR light-weight robot

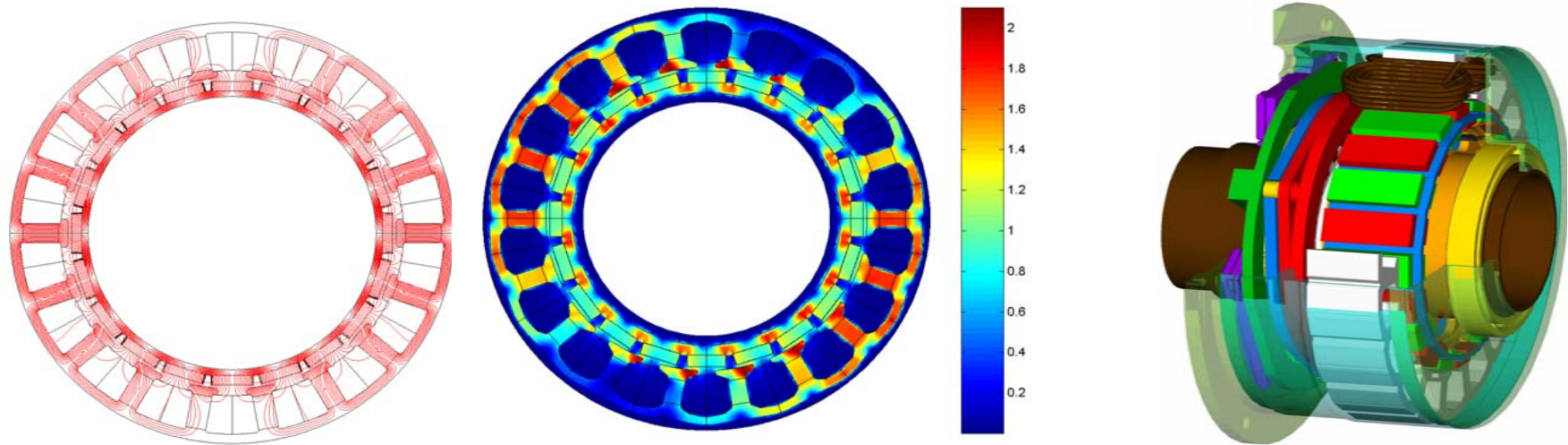
- 7 Axes
- Weight: 13.5 kg
- Payload: 13.5 kg



# Modular Robot Design

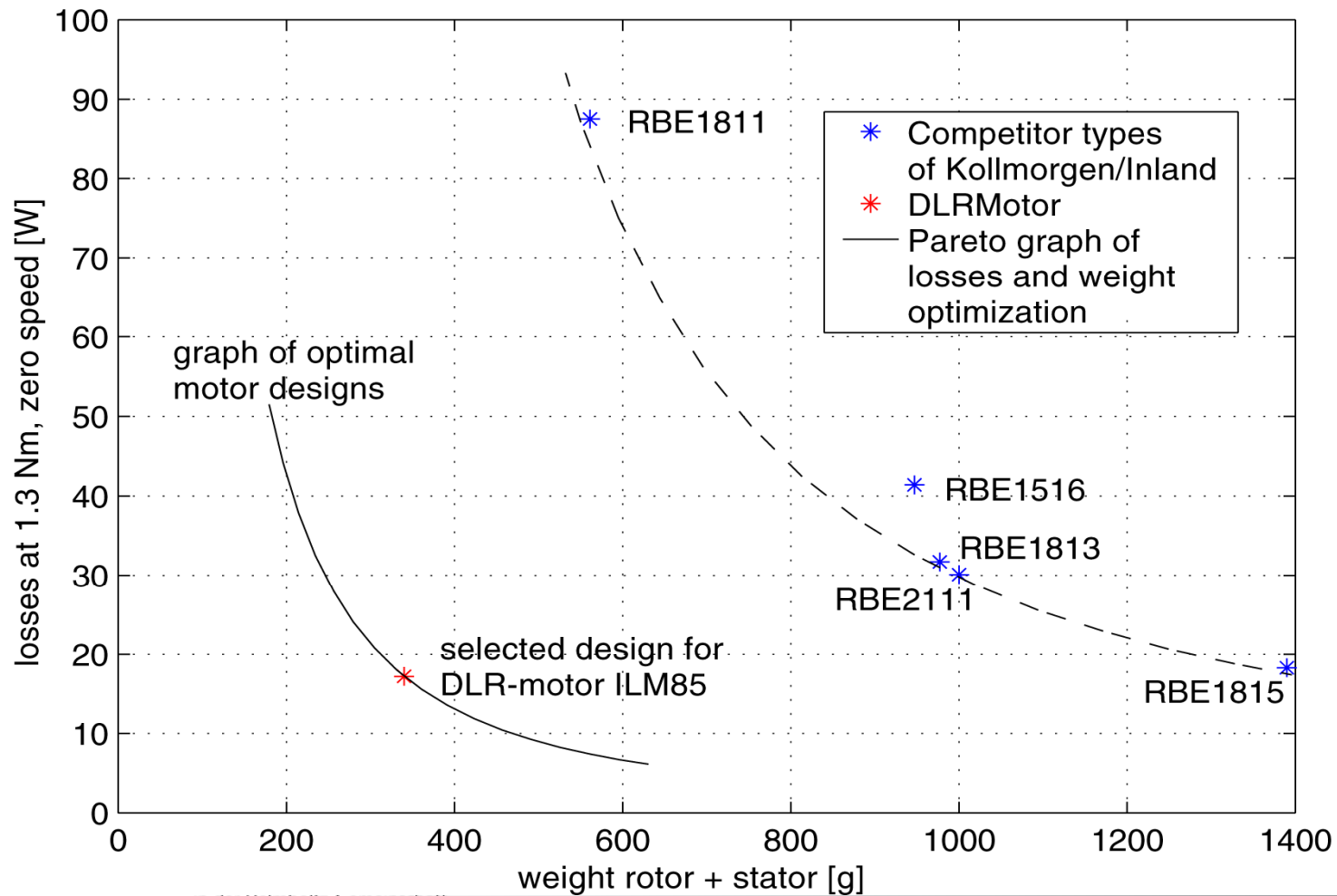


# Concurrent Engineering- via multidisciplinary simulation to an optimized motor design

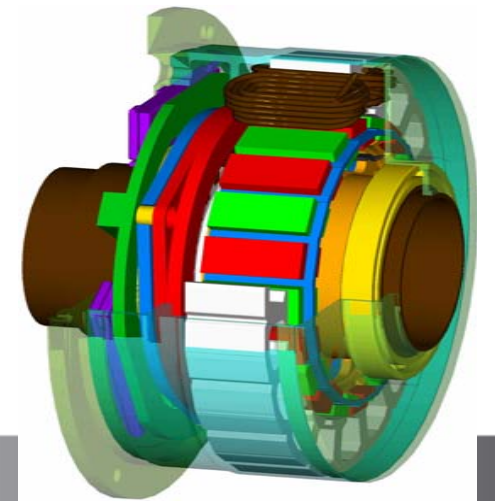




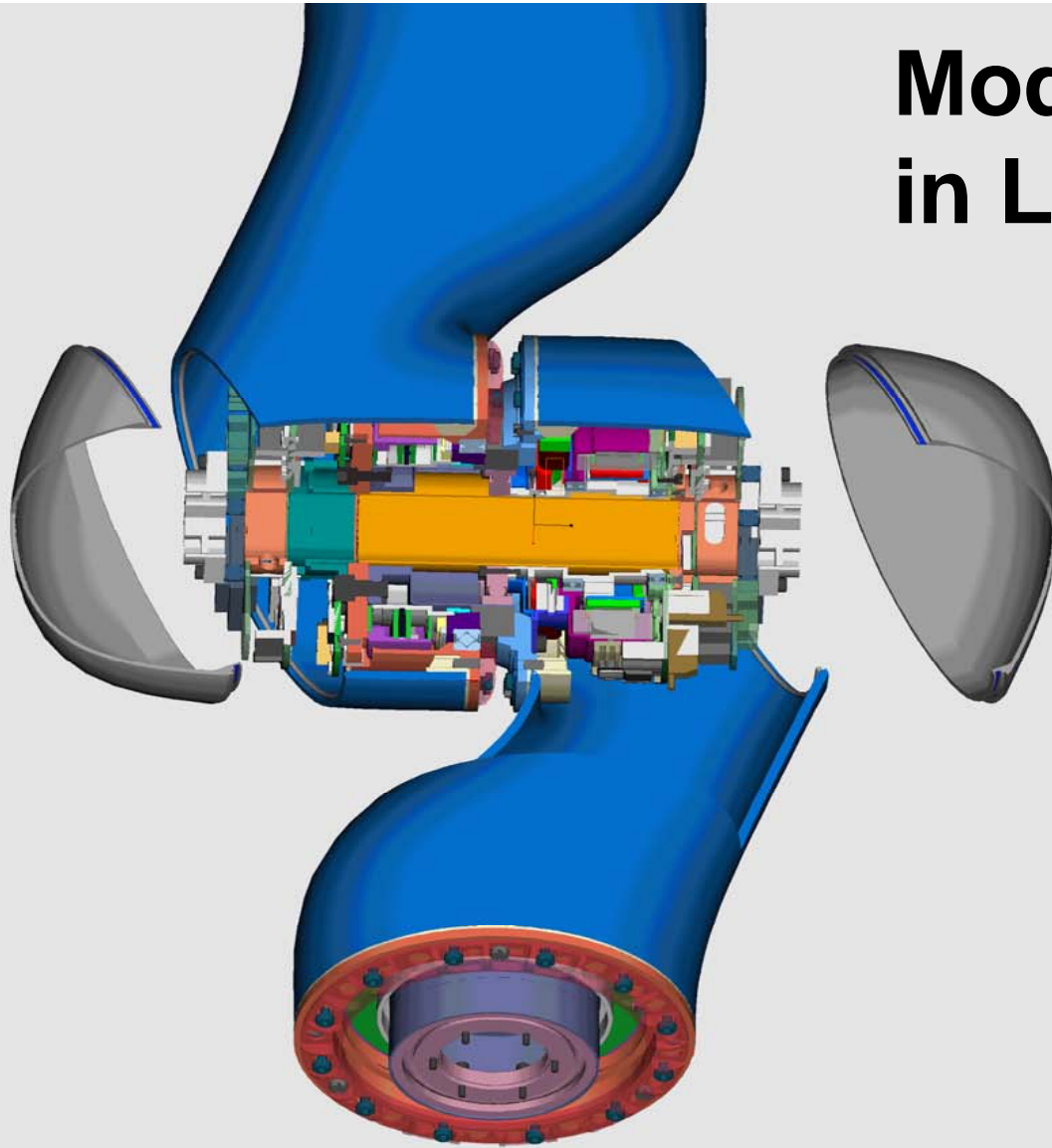
# DLR`s new ROBODRIVE- half weight, half losses



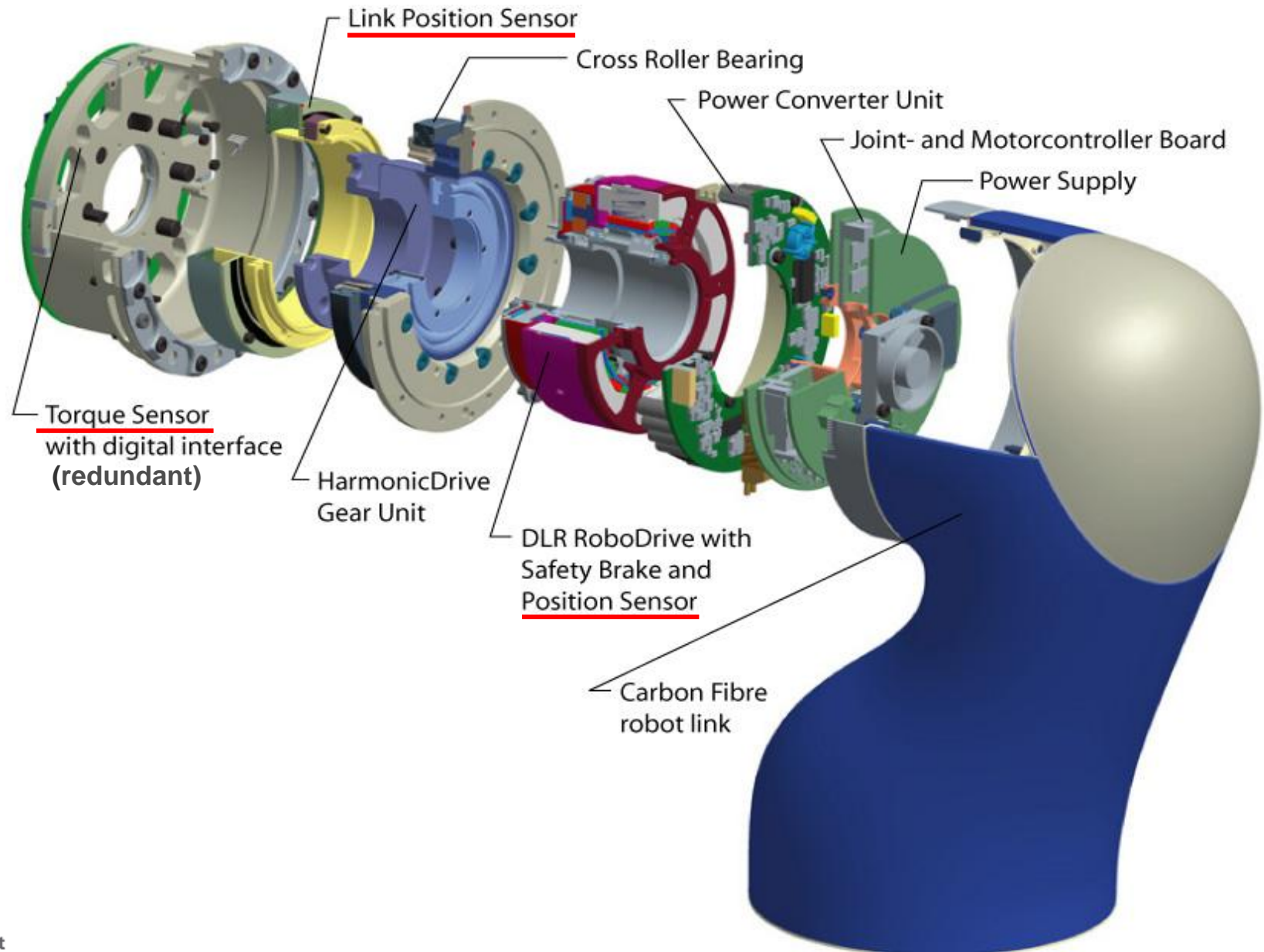
in der Helmholtz-Gemeinschaft



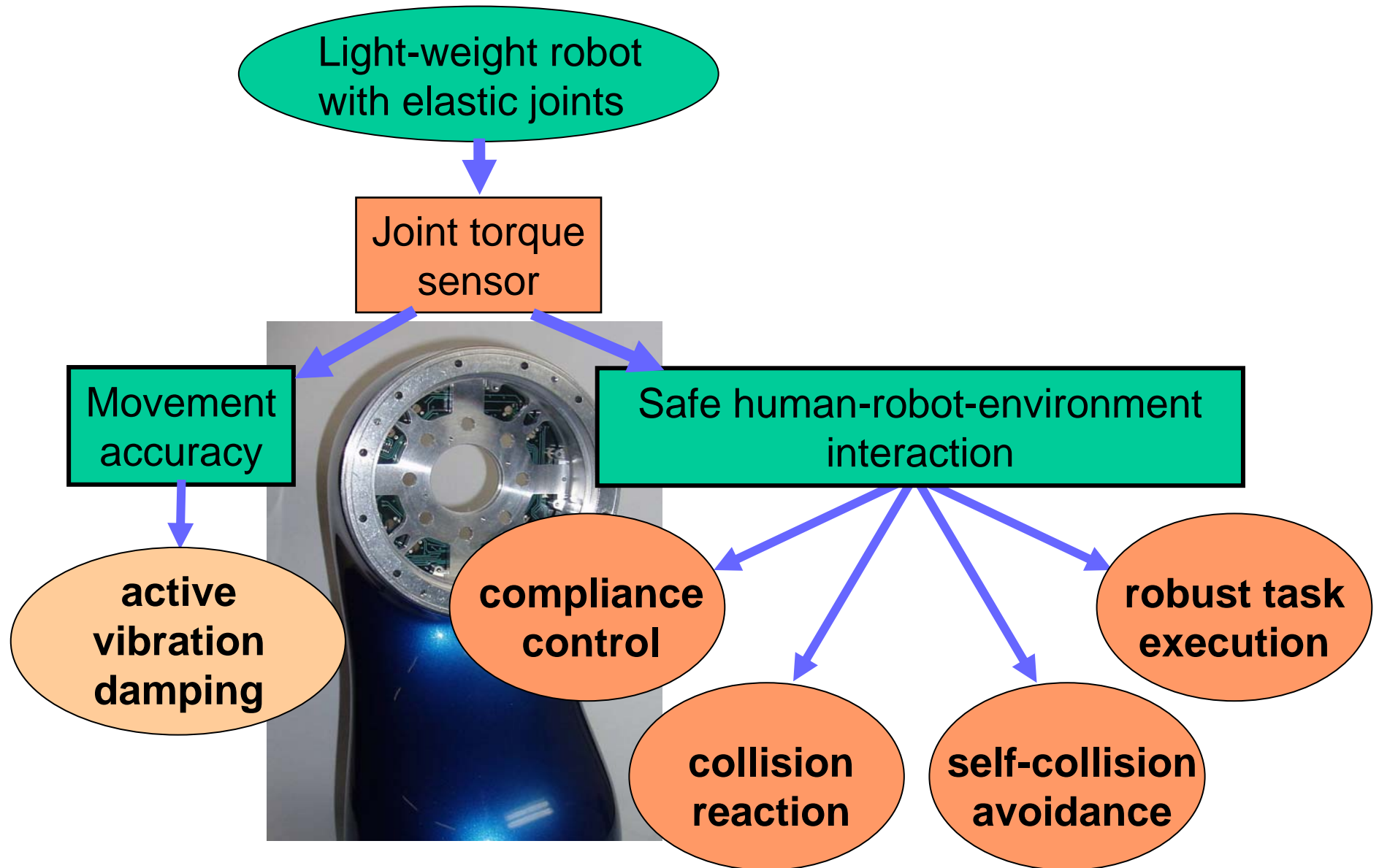
# Modular drives in LWR III



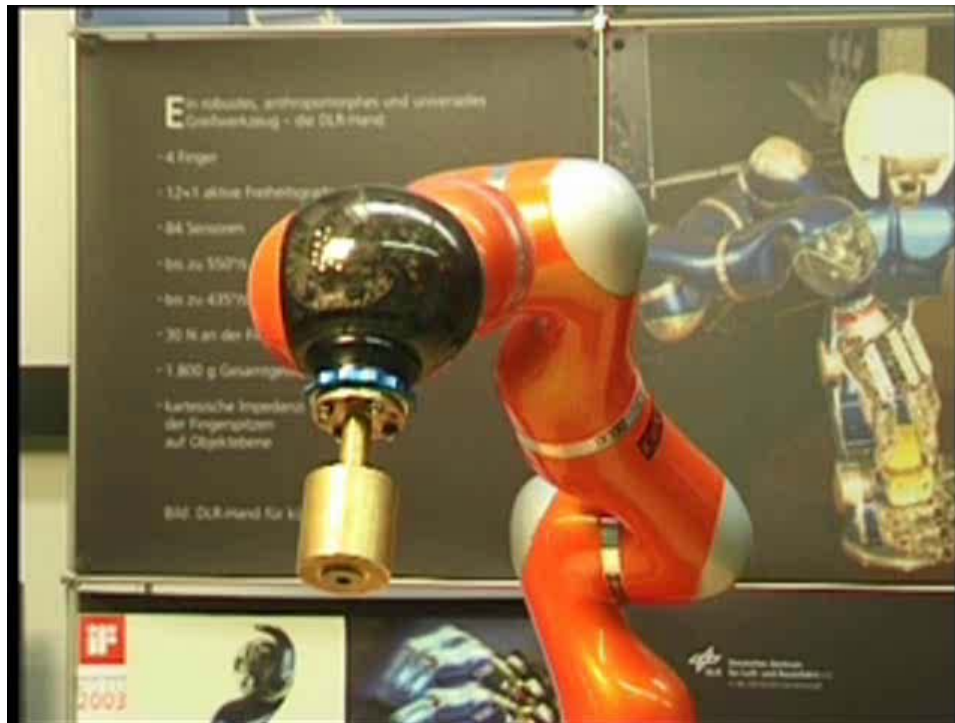
# Mechatronic Joint Design



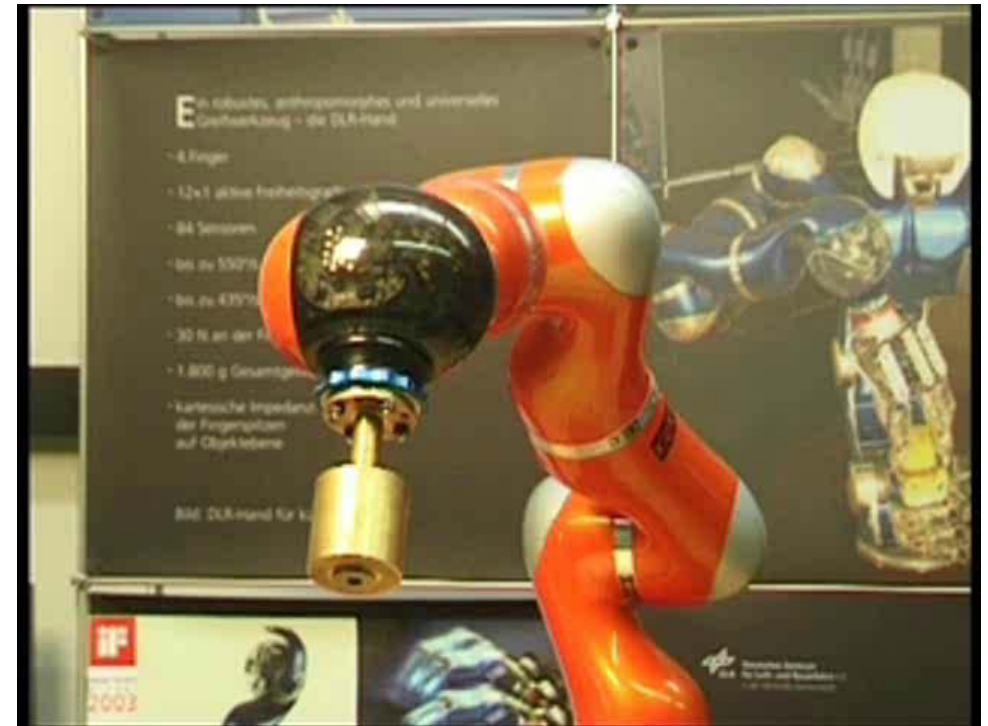
# Control components



# Vibration Damping



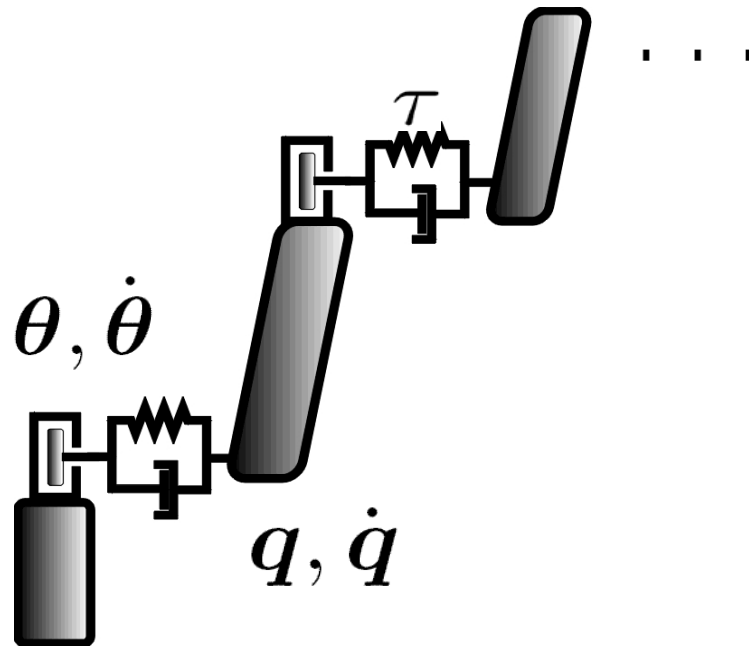
Vibration Damping ON



Vibration Damping OFF

**Robot reaches the dynamics and accuracy of an industrial arm  
(according to KUKA ISO-Tests)**

# Model of the flexible joint robot



possible state vector:

$$x_1^T = \{\theta, \dot{\theta}, q, \dot{q}\}$$

used state vector:

$$x^T = \{\theta, \dot{\theta}, \tau, \dot{\tau}\}$$

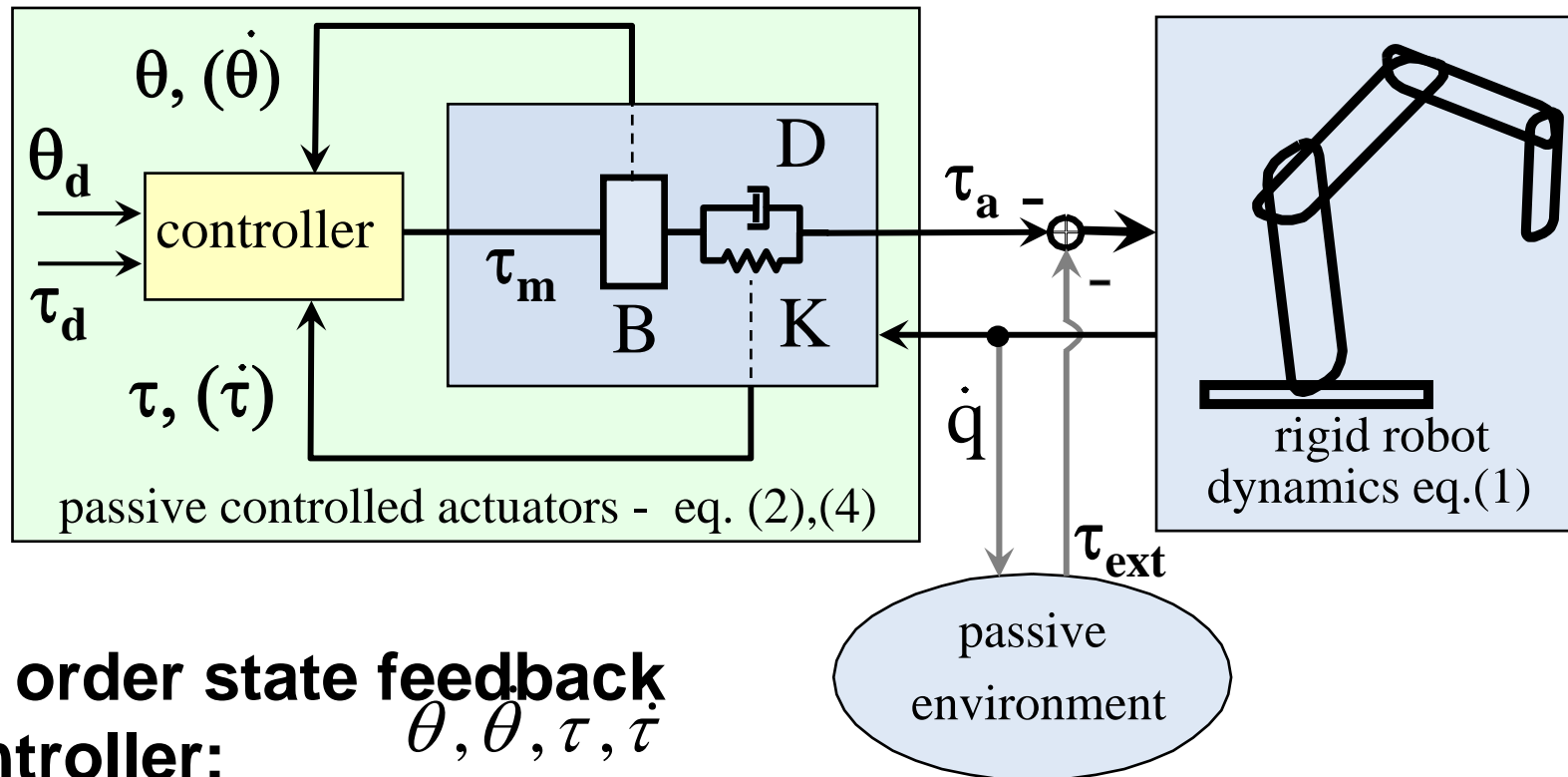
$$M(q)\ddot{q} + C(q, \dot{q})\dot{q} + g(q) = \underline{\tau + DK^{-1}\dot{\tau}} + \tau_{ext}$$

$$B\ddot{\theta} + \underline{\tau + DK^{-1}\dot{\tau}} = \tau_m$$

$$\tau = K(\theta - q)$$



# Joint Level Control



**4th order state feedback controller:**  $\theta, \dot{\theta}, \tau, \dot{\tau}$

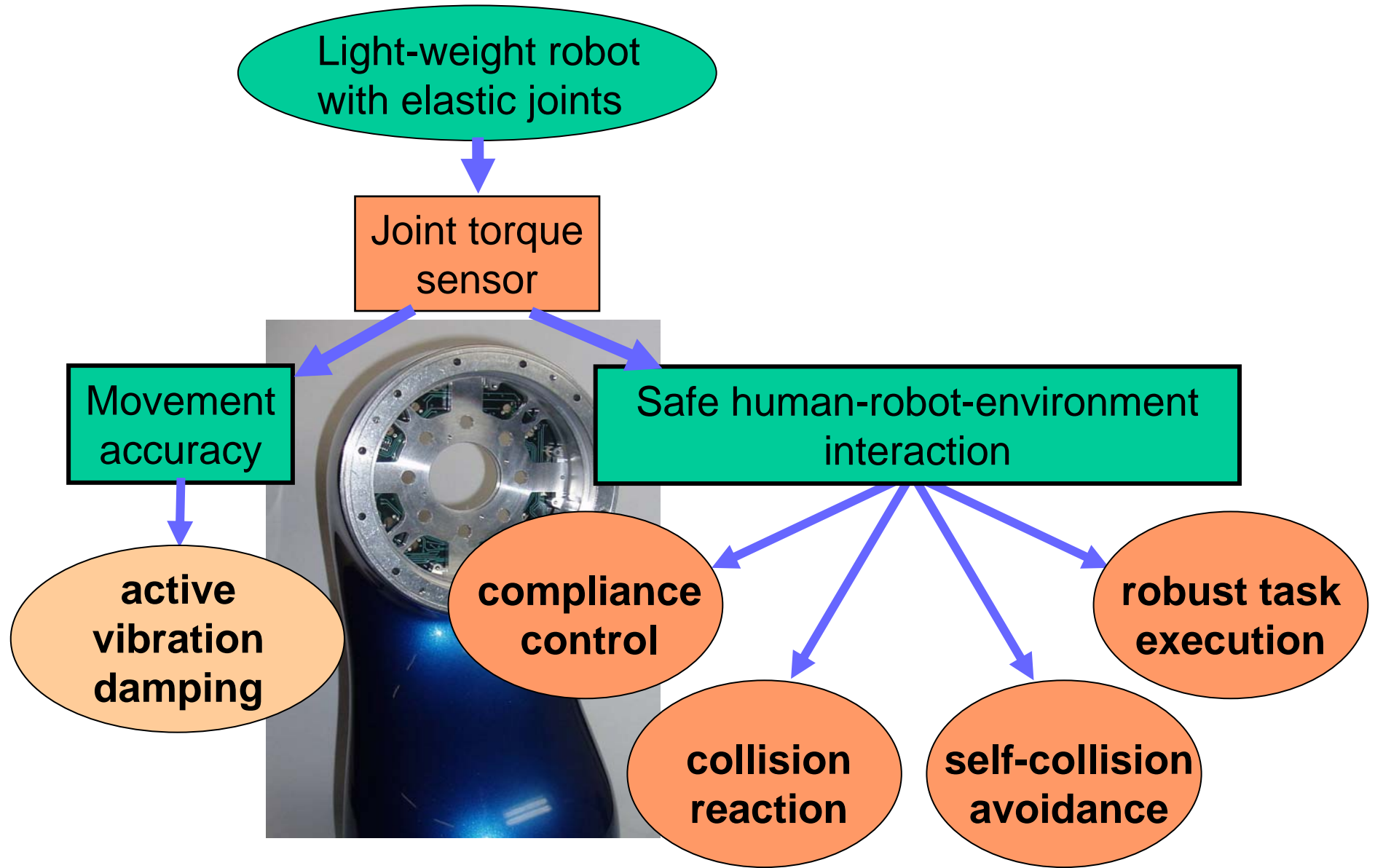
same structure used for

- torque control
- position control
- impedance control





# Control components



# Torque Control with Gravity Compensation



# Cartesian Impedance Controller

Generalization of approaches from rigid robots to the flexible case

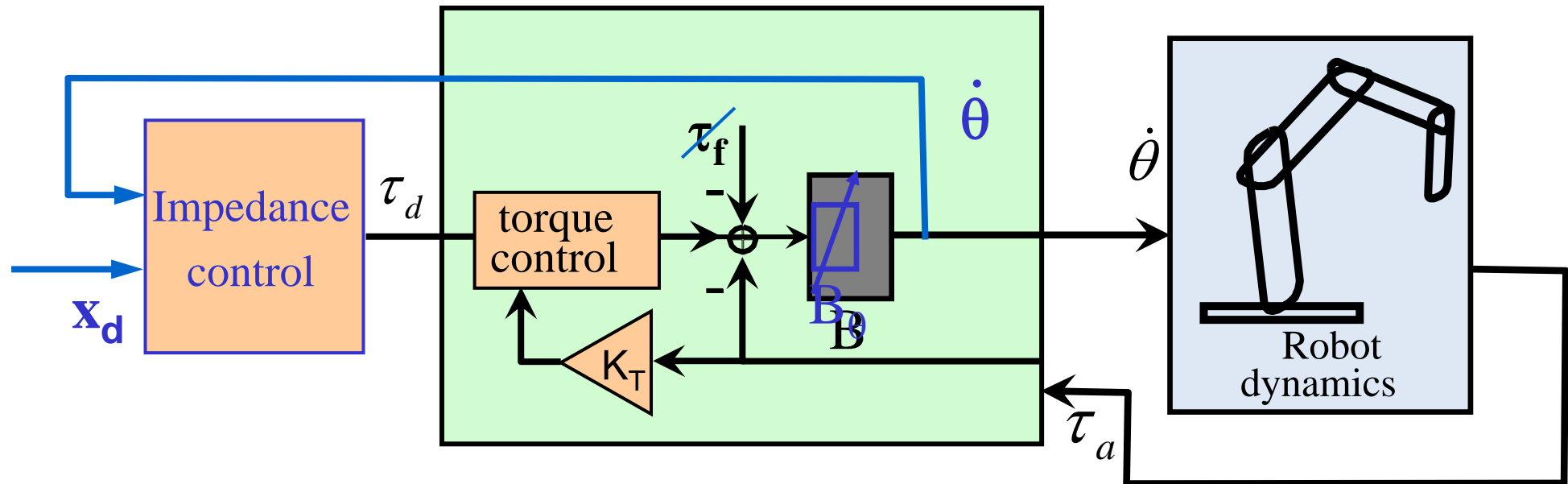
- Shaping the **potential energy - collocated feedback**
  - Asymptotic stabilization around  $x_d$  ( $\tau_{ext} = \mathbf{0}$ )
  - Implementation of the desired compliance relationship ( $\tau_{ext} \neq \mathbf{0}$ )
  - Feedback of  $\theta, \dot{\theta}$
- Shaping of the **kinetic energy - noncollocated feedback**
  - Damping of vibrations => increased performance
  - Feedback of  $\tau, \dot{\tau}$  (torque controller)

=> Full state feedback



# Cartesian Impedance Control

Unified approach for torque, position and impedance control on Cartesian and joint level

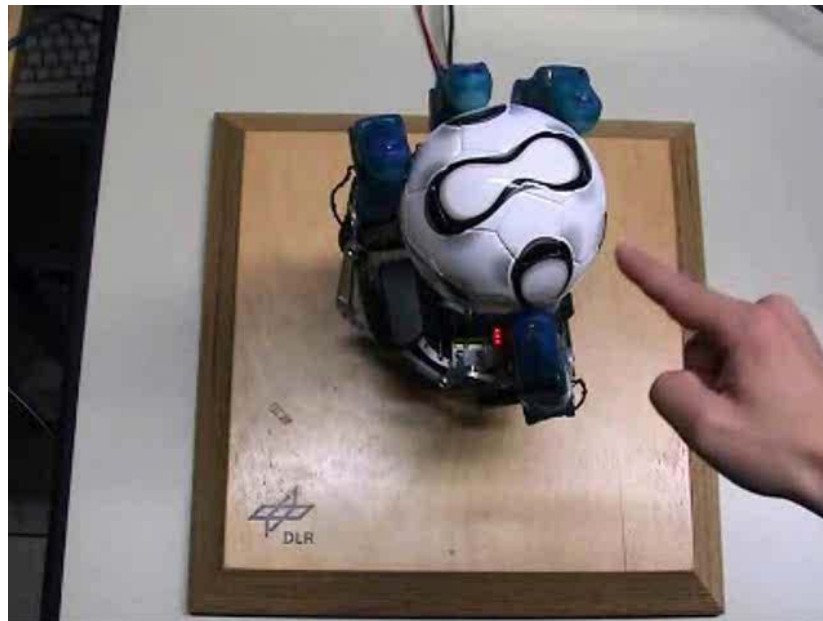
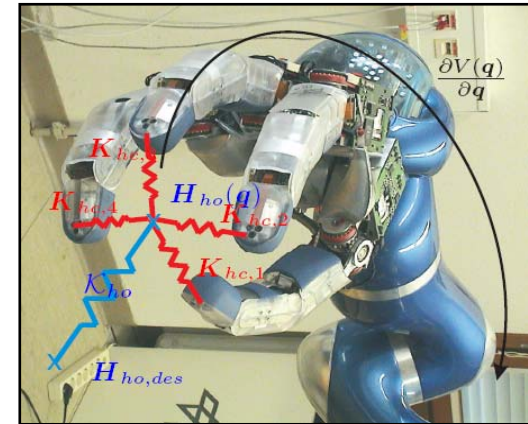


**Passivity  $\longrightarrow$  Robustness in contact with the environment**

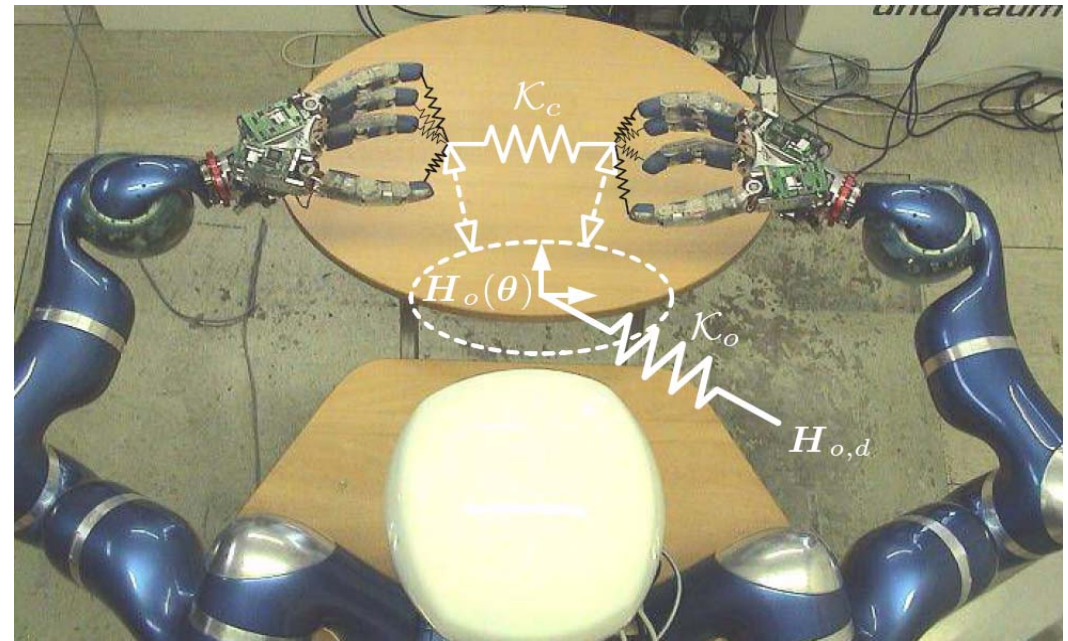
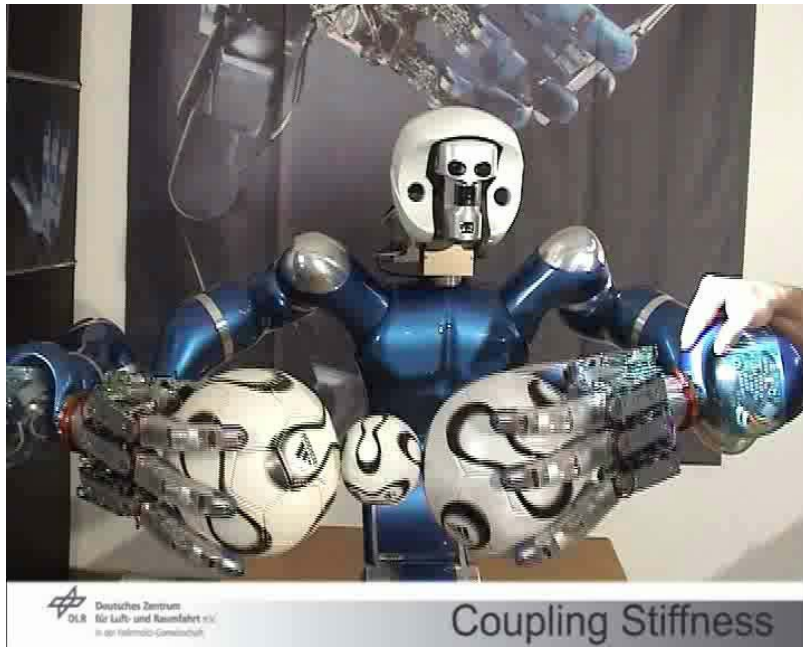


# DLR Hand II – Impedance Control

- Joint impedance Control
- Cartesian Impedance Control
- Object Impedance Control



# Impedance Control for Two Handed Manipulation



$$\tau_d = \bar{g}(\theta) - \frac{\partial V(\theta)}{\partial \theta} - D(\theta)\dot{\theta}$$

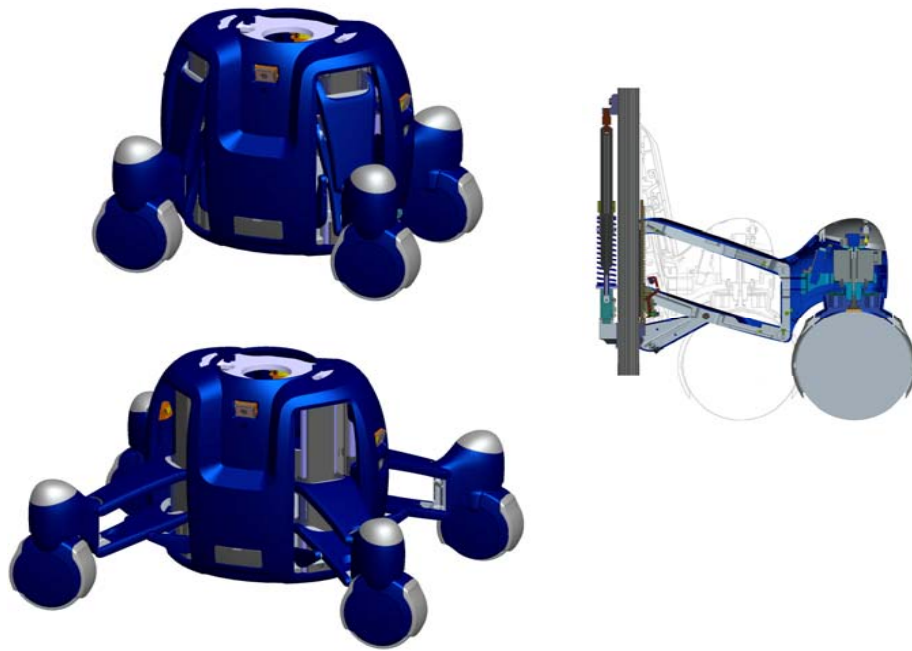
Gravity  
compensation

Stiffness term

Damping term

1ms control cycle for the whole system

# Development and Control of the Omni-Directional, Mobile Platform



- Wheels can be independently retracted  
(variable support area)
- 8 actuators
  - 4 steering actuators
  - 4 wheel actuators
- Passive suspension - lockable

Fixed leg length: all joint axes intersect in the Instantaneous Center of Rotation (ICR)

For leg extension while moving no ICR exists – controller generalizations were needed



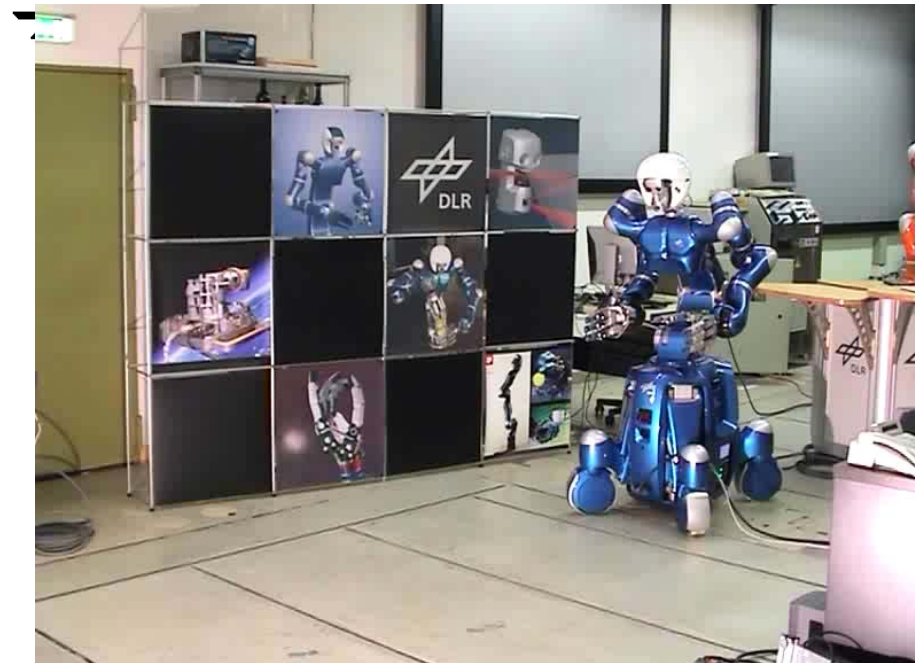
# Development and Control of the Omni-Directional, Mobile Platform



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- 8 actuators
  - 4 steering actuators
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Fixed leg length: all joint axes intersect in the Instantaneous Center of Rotation (ICR)

For leg extension while moving no ICR exists – controller generalizations were needed





# Human-Robot-Interaction

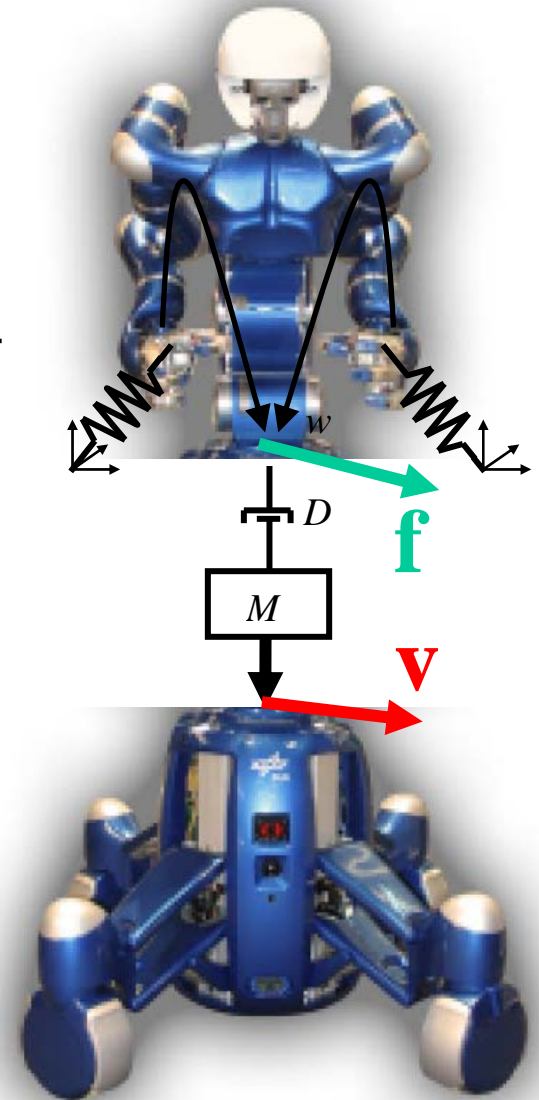
## Compliant Control of the entire Robot



**Rollin' Justin**

- 53 active dof
- 150 kg

Admittance Control Impedance Control



# Collision Avoidance

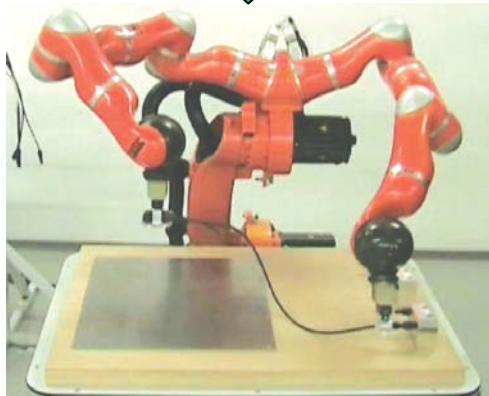
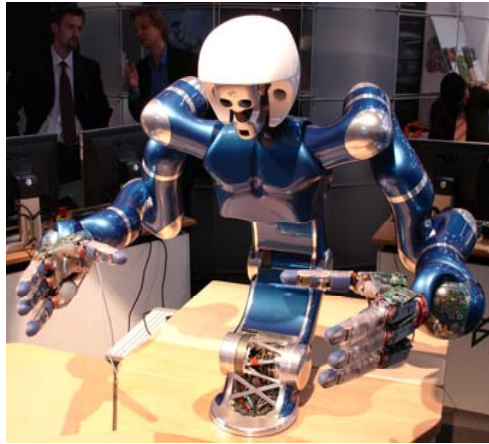
Avoidance of collisions with repulsive potentials

Compatible with the passivity based approach

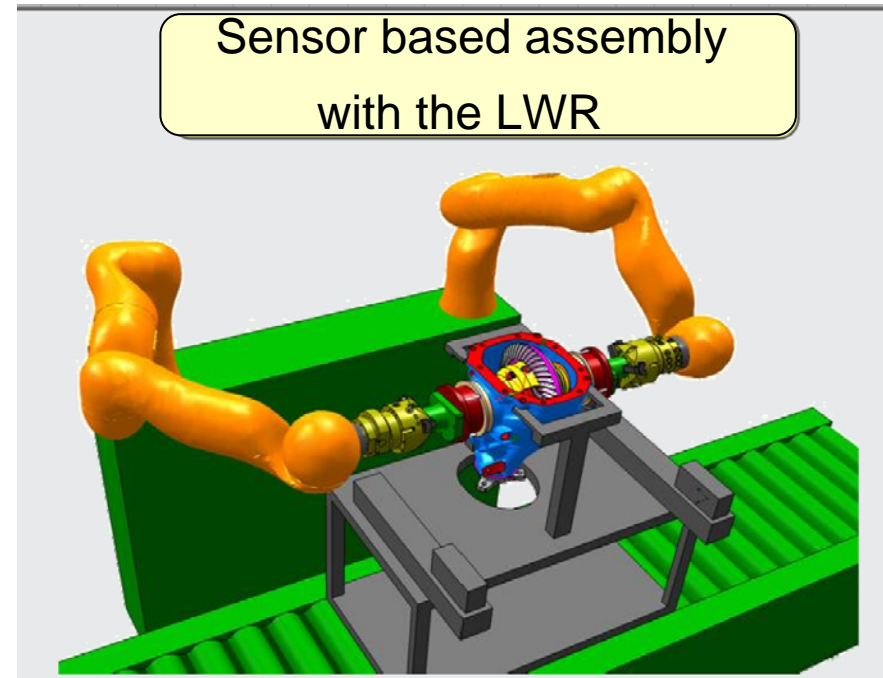
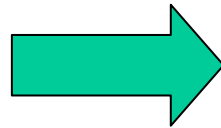


Cooperation with Univ. of Naples  
(Lab of Bruno Siciliano)

# First Application of the Technology in Automotive Industry



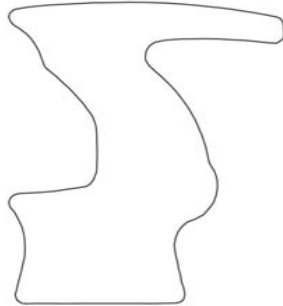
KUKA Demonstrator



- Gearbox assembly tests since March 2009
- Production starting from September 2009



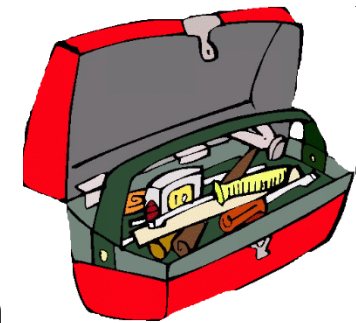
# Basic Idea



Geometrical Model  
(from image processing / CAD)

Additional information:

- tolerance
- material properties
- Robot and camera accuracy
- additional constraints



## Assembly Planning Toolbox

```
351 ; dann Flugstrategie steigertagesteuert aufbauen
352 SetUmschlaglogos()
353 PTF XlogoFAPAS:(x 0, y 0, z -20, a 0, b 0, c 0)rotOFF
354 WAIT SEC 0.3
355
356 ; Platz schon belegt
357 IF ((EFOS_ACT.Z - XlogoFAPAS.Z) > 35) THEN
358   ; rausziehen
359   PTF XlogoFAPAS:(x 0, y 0, z -10, a 0, b 0, c 0)rotOFF
360   Inverse[2] = TRUE
361   done = TRUE
362 ELSE
363   LIN XlogoFAPAS:(x -5, y -4, z -20, a 0, b 0, c 0):(x 0, y 0, z 0,
364   LIN XlogoFAPAS:(x -5, y -4, z -1, a 0, b 0, c 0):(x 0, y 0, z 0, a
365   LIN XlogoFAPAS:(x 10, y -4, z 2, a 0, b 0, c 0):(x 0, y 0, z 0, a
366   LIN XlogoFAPAS:(x 10, y 0, z 2, a 0, b 0, c 0):(x 0, y 0, z 0, a 0
367   WAIT SEC 0
368   LIN EFOS_ACT:(x 0, y 0, z 20, a 0, b 0, c 0)
369   LIN EFOS_ACT:(x -10, y 0, z 20, a 0, b 0, c 0)
```

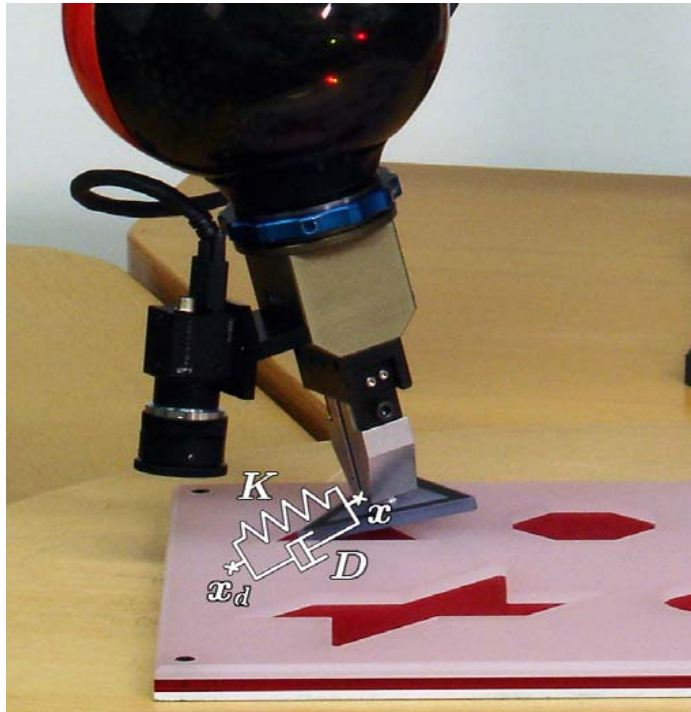
KRL code

Online-Data:

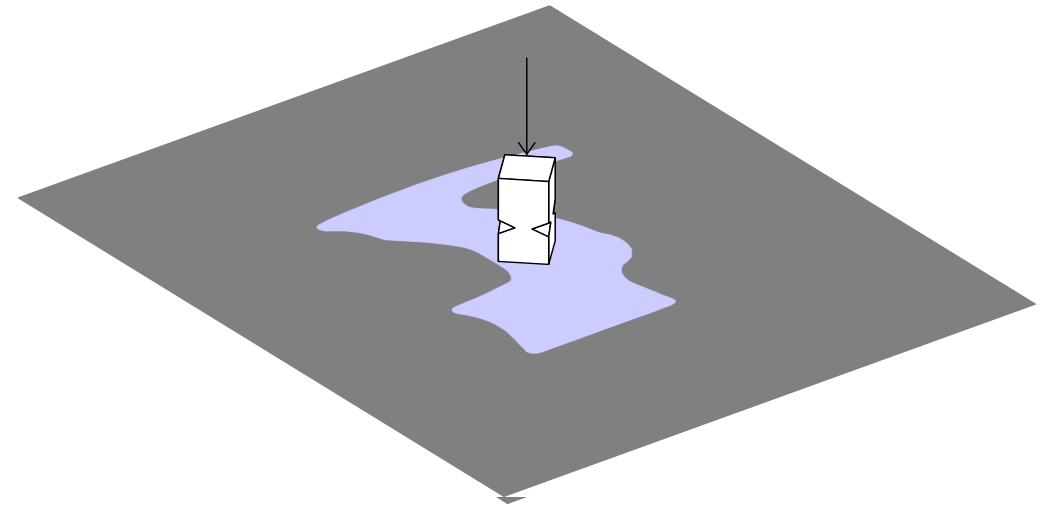
- Position estimation
- Workspace limitations
- Robot configuration
- additional sensor data



# Vision and Impedance Based Assembly

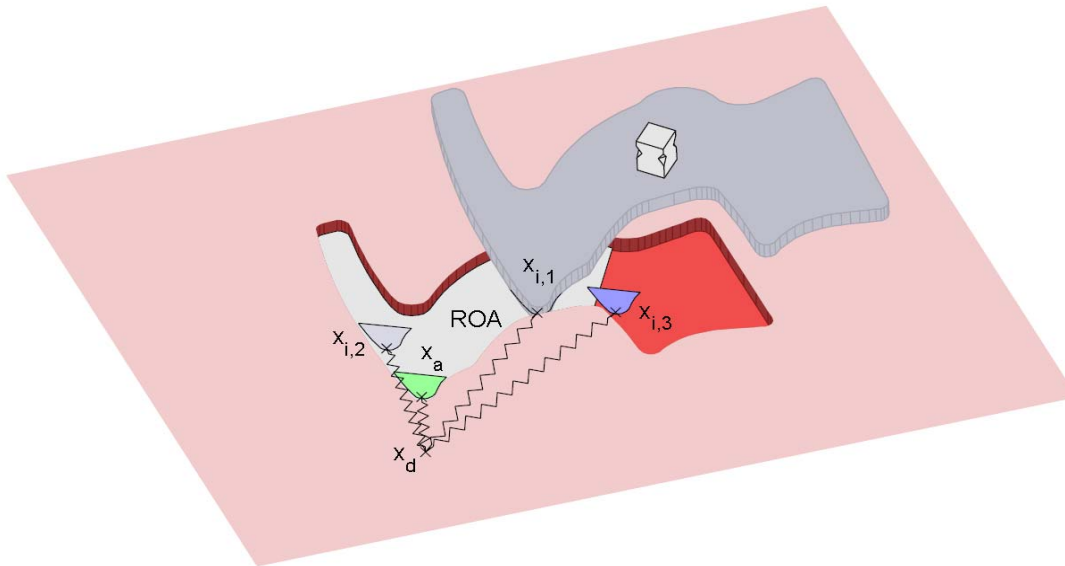


$$F = -K(x - x_d) - D\dot{x}$$



➤ Problem statement : Automatically find and program the optimal strategy

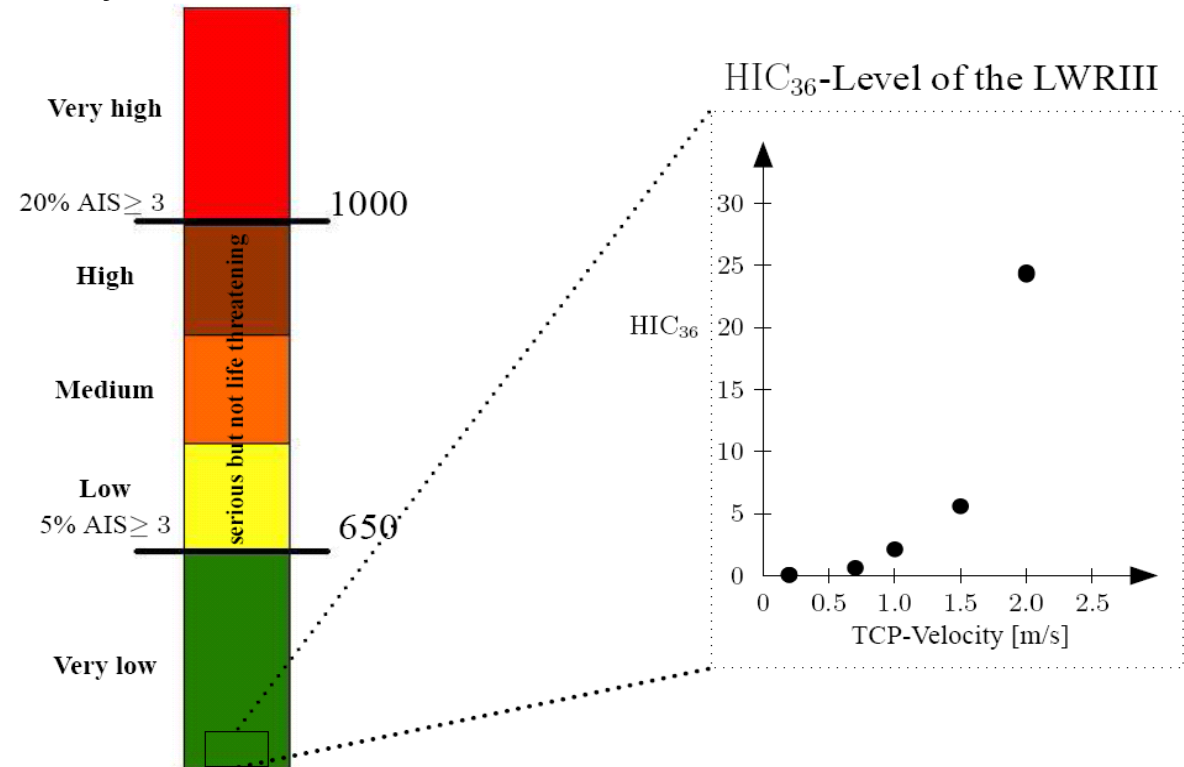
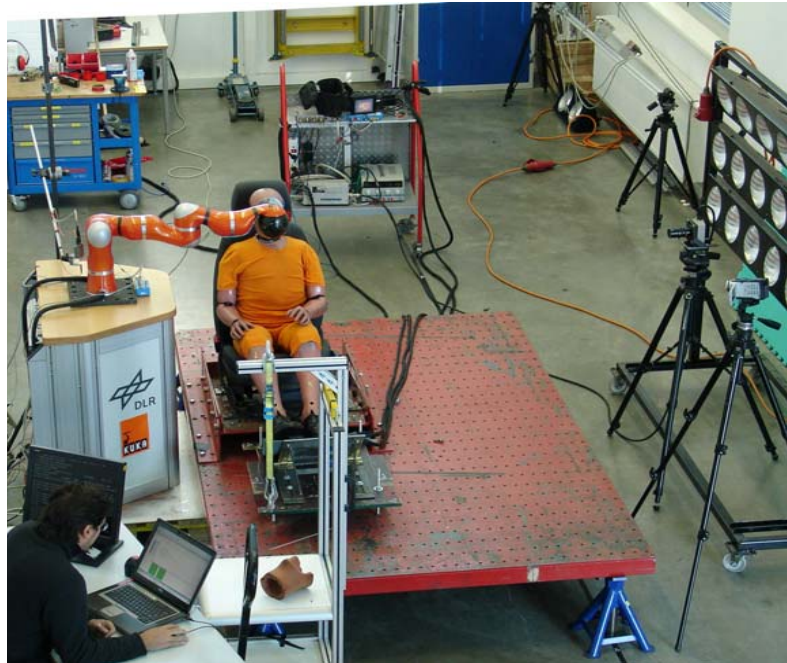
# Regions of Attraction (ROA)



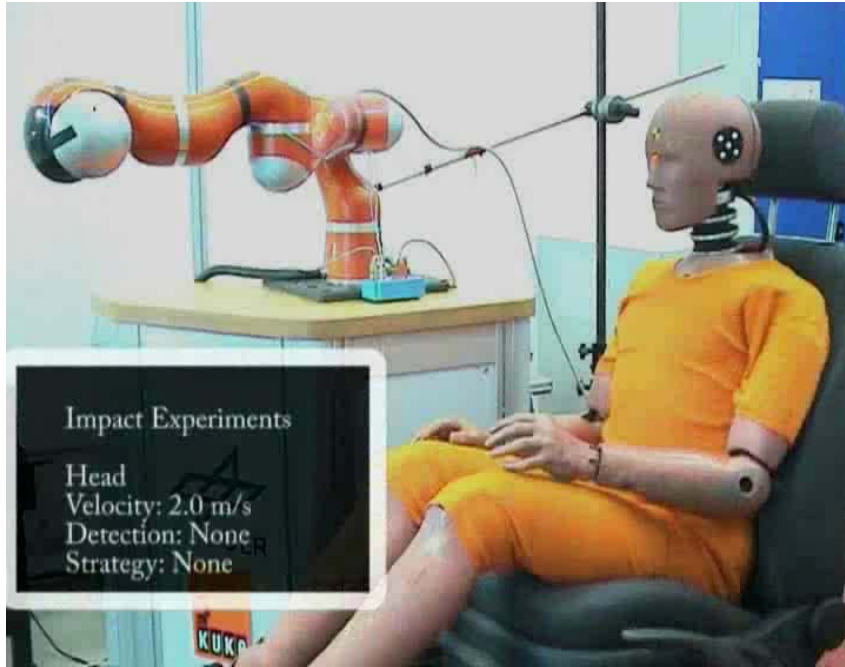
- The contact point with maximal ROA provides maximal robustness w.r.t. sensor and mode uncertainties
- A local Lyapunov Based convergence analysis is possible based on the impedance controlled robot and the contour geometry

# How Dangerous is the Robot Really?

First collision experiments with standardized methods for evaluation of injury potential and related safety measures in robotics

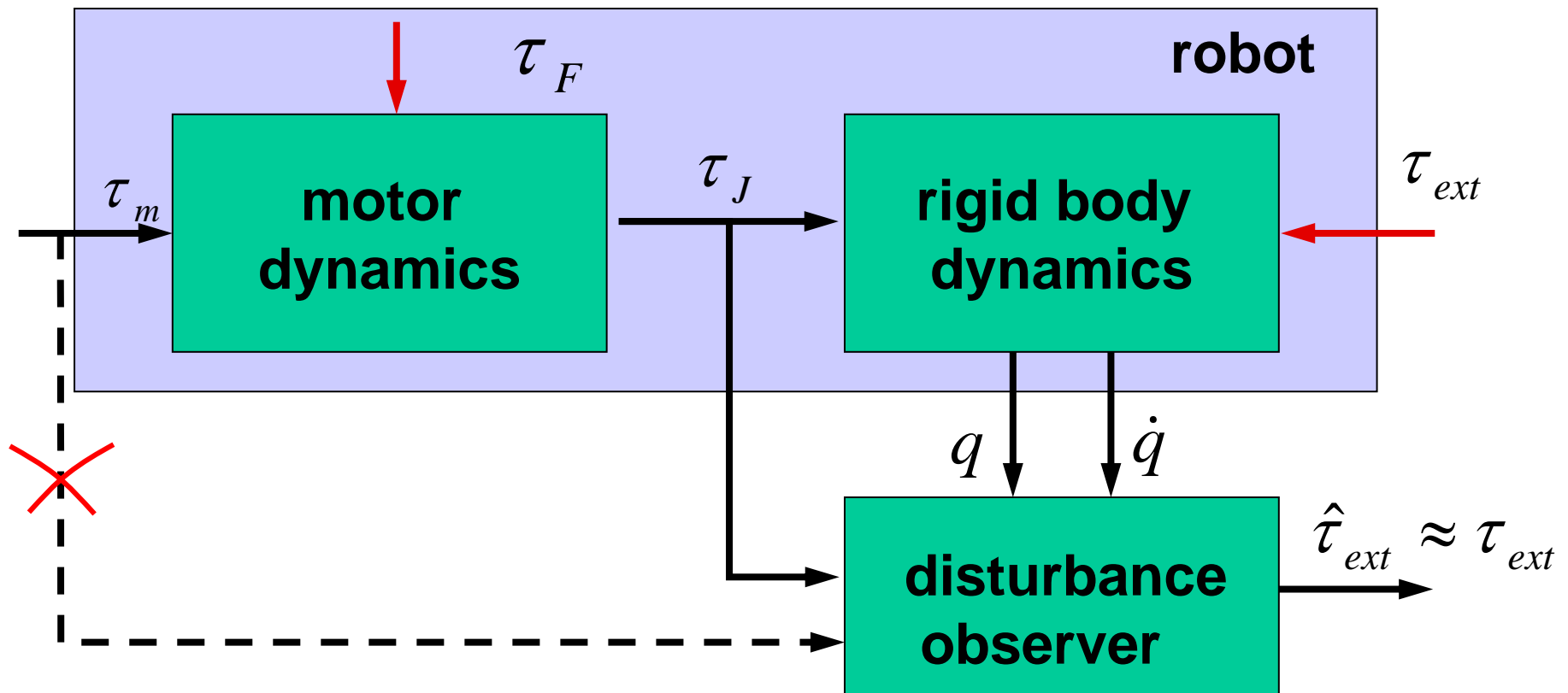


For all evaluated criteria, the LWR proved to be in the lower quarter of the green, uncritical area





# Disturbance Observer for Collision Detection

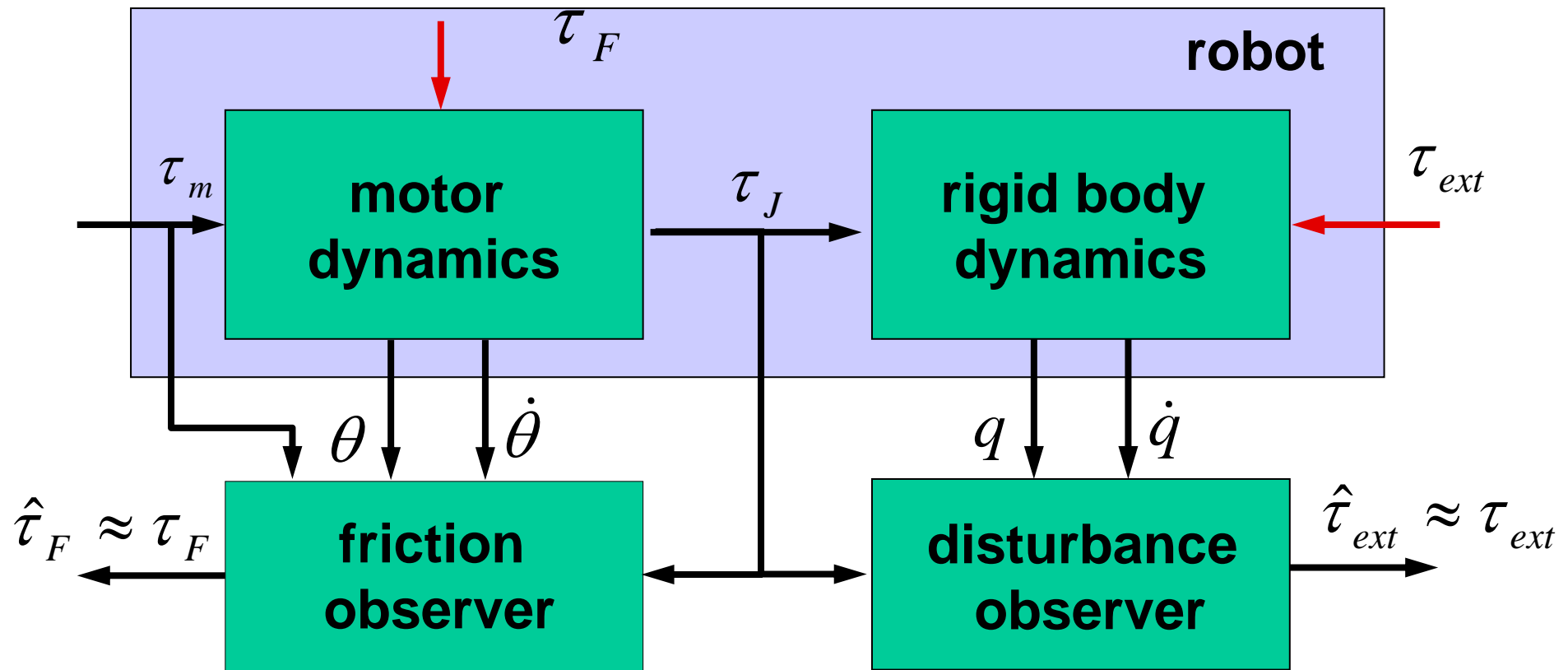


IROS'06

with Alessandro De Luca



# Disturbance Observer for Collision Detection and Friction Compensation



IROS'08

with Alessandro De Luca

# Joint Flexibility – a **Feature**, not a **Drawback**

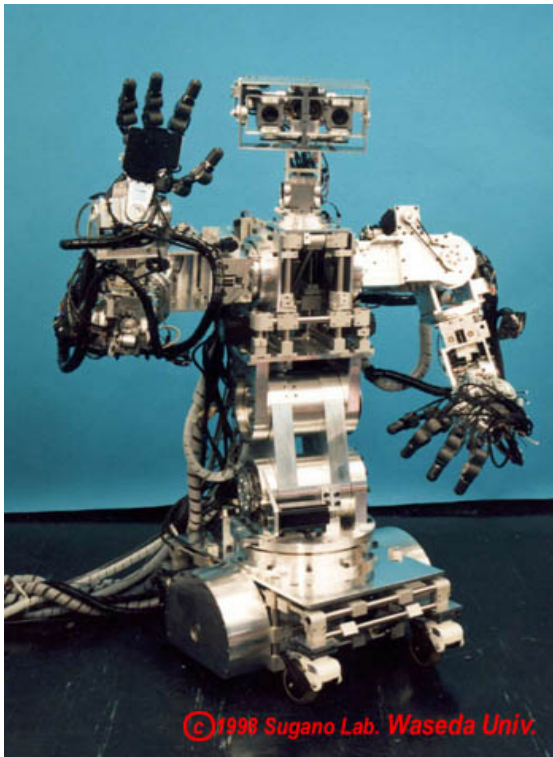
• **Constant Compliance:**  
Series Elastic Actuators (G. Pratt)

Benefits are **INTRINSIC** to the arm design w.r.t.:

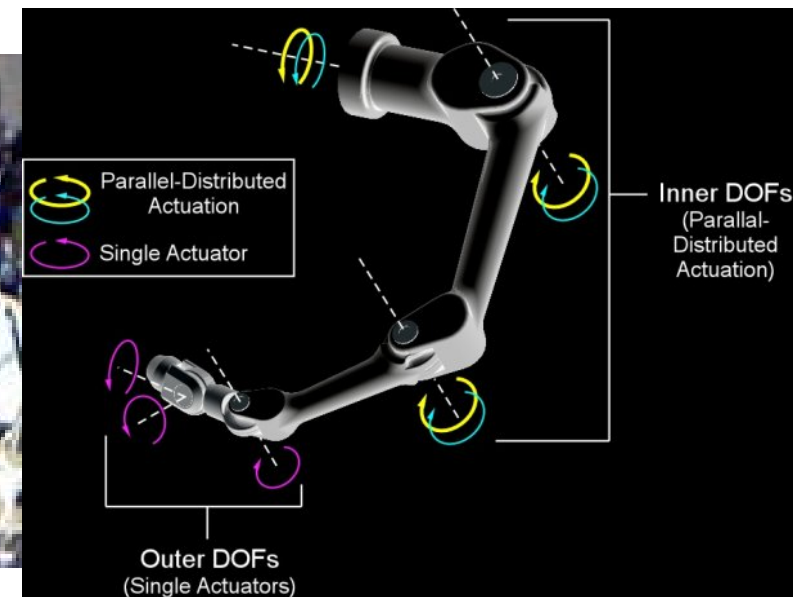
- Robust manipulation in unknown environments
- Dynamic Performance and energy efficiency
- Mechanical robustness in case of failure or impact
- Safe interaction with humans



• **Variable Impedance Actuators (VIA):**



(Bicchi, Univ. of Pisa)



(Khatib, Stanford Univ.)

# Rigid vs. Compliant Actuation

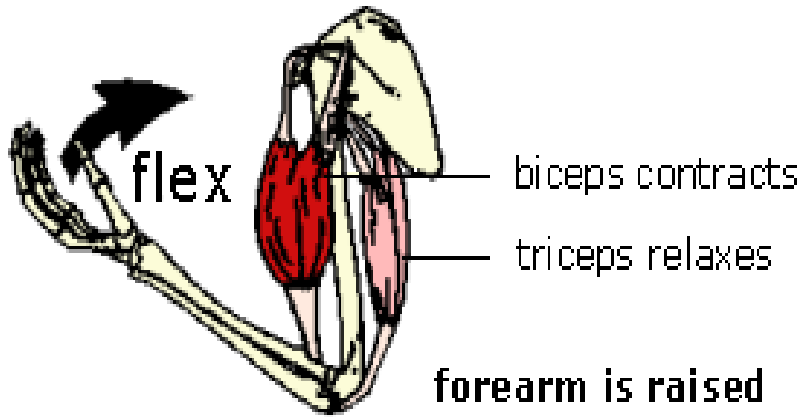


One of today's most advanced humanoid

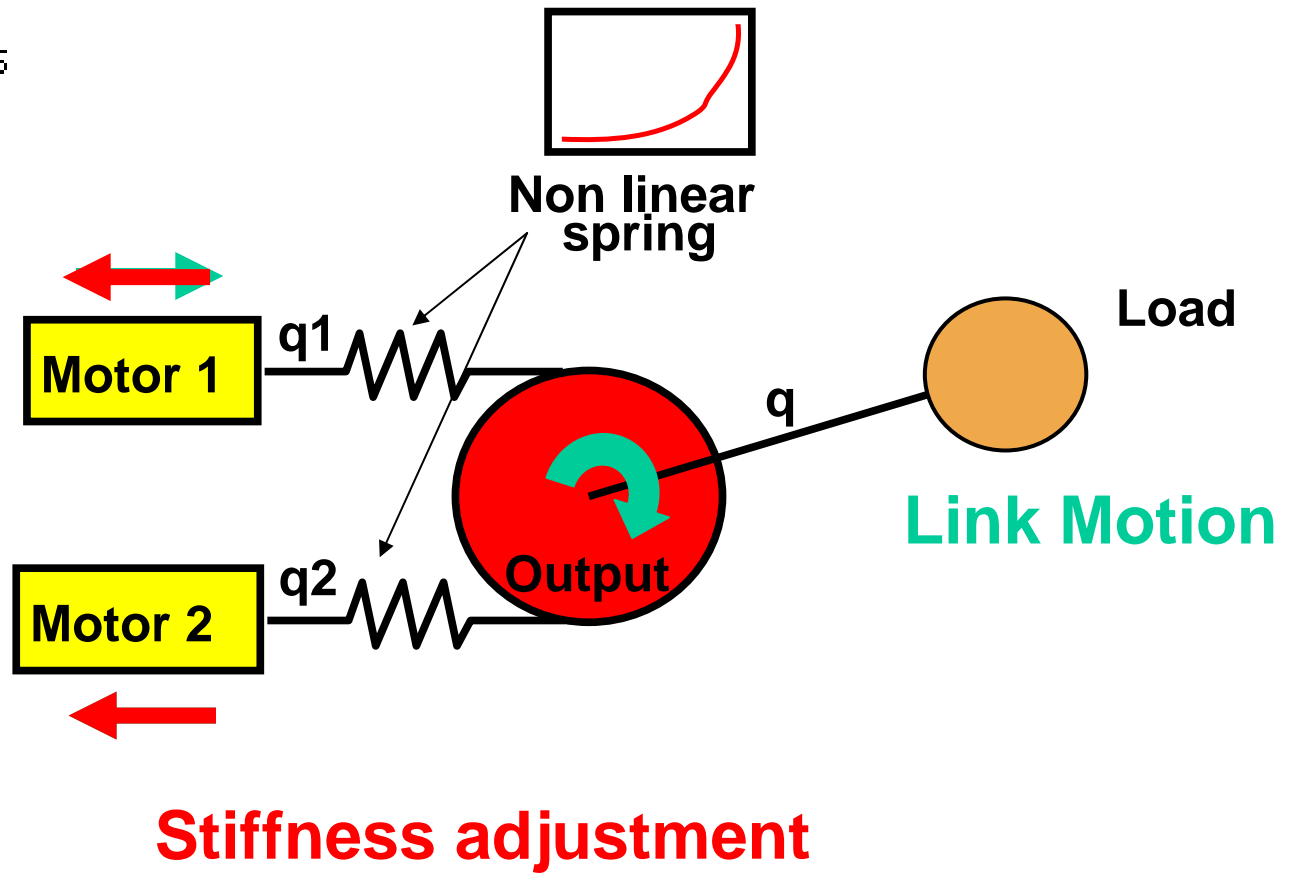


Human top performance

# The Principle of VIA

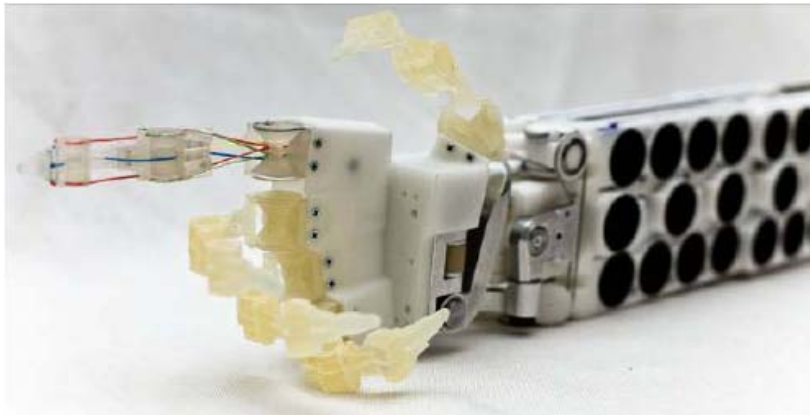


The antagonistic concept

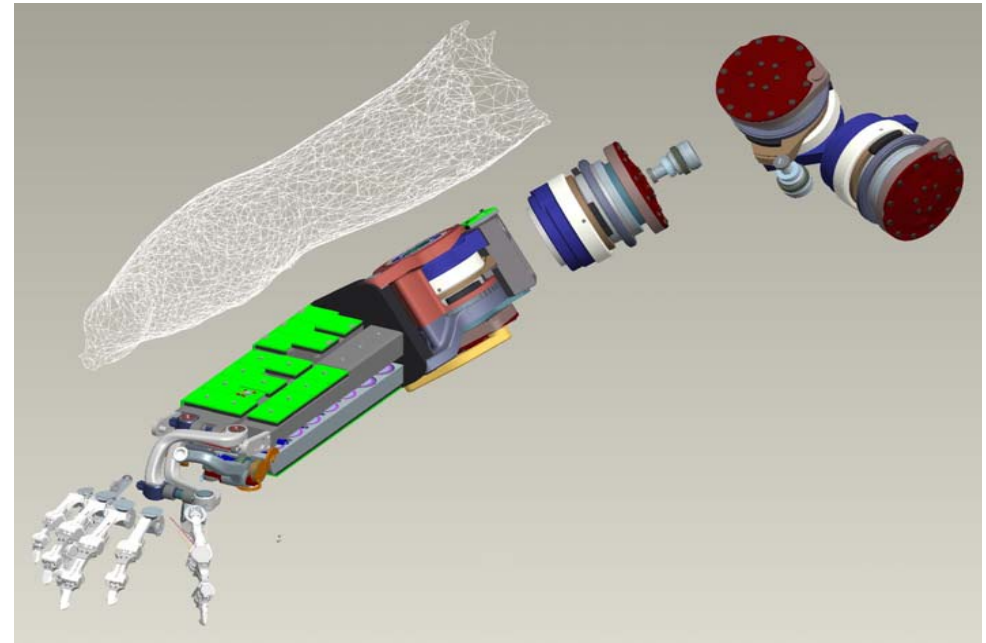


# The New DLR Hand-Arm-System

## VIA – Variable Impedance Actuation



new VIA Hand  
(38 Motors)



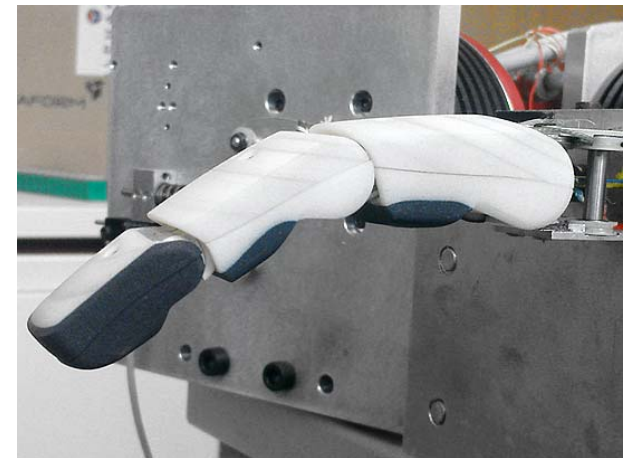
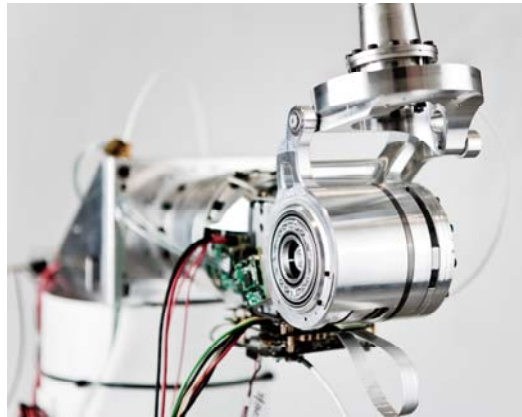
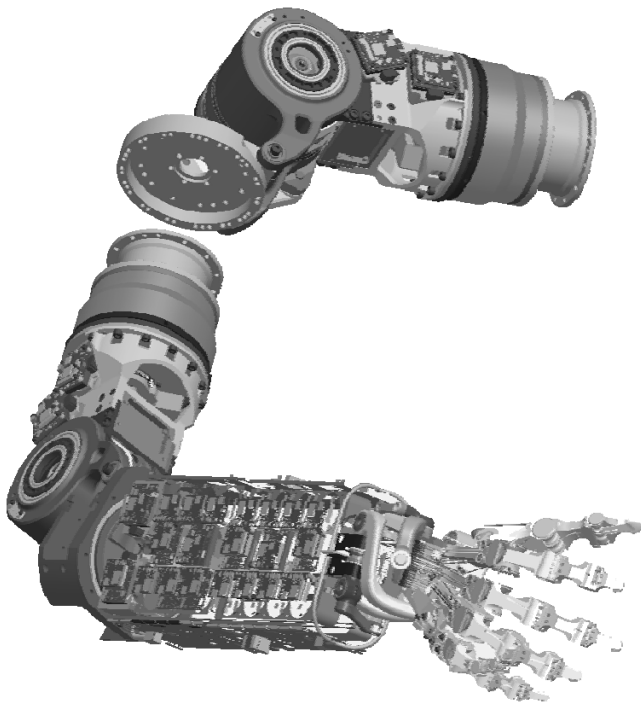
Sketch of VIA Arms

Extension of the passivity based control approaches to the VIA robots:

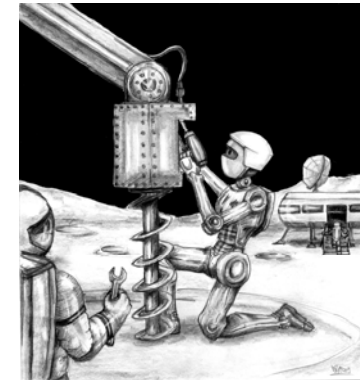
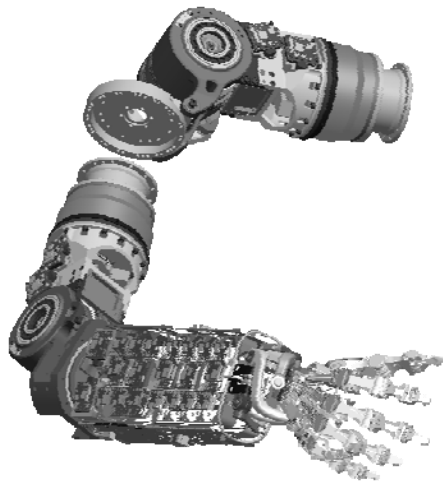
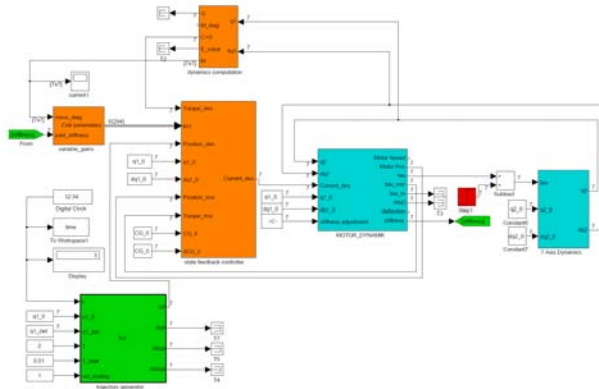
- Variable, nonlinear stiffness
- Strongly coupled joints

# Anthropomorphic Hand-Arm-System

- Size, force and dynamics of a human arm/hand
- Variable stiffness
- *54 motors, 108 position sensors*



# A Hand-Arm System for Space Robot Assistance



Extension of the passivity based control approaches to the VIA robots:

- Variable, nonlinear stiffness
- Strongly coupled joints



# Control of VIA Joints

The joints have very low intrinsic damping

useful for cyclic movements  
involving energy storage  
(running or throwing)

damping of the arm for fast,  
fine positioning tasks has to be  
realized by control.

- Ensuring the achievement of the desired link position with motor position based control.
- Providing the desired stiffness property.



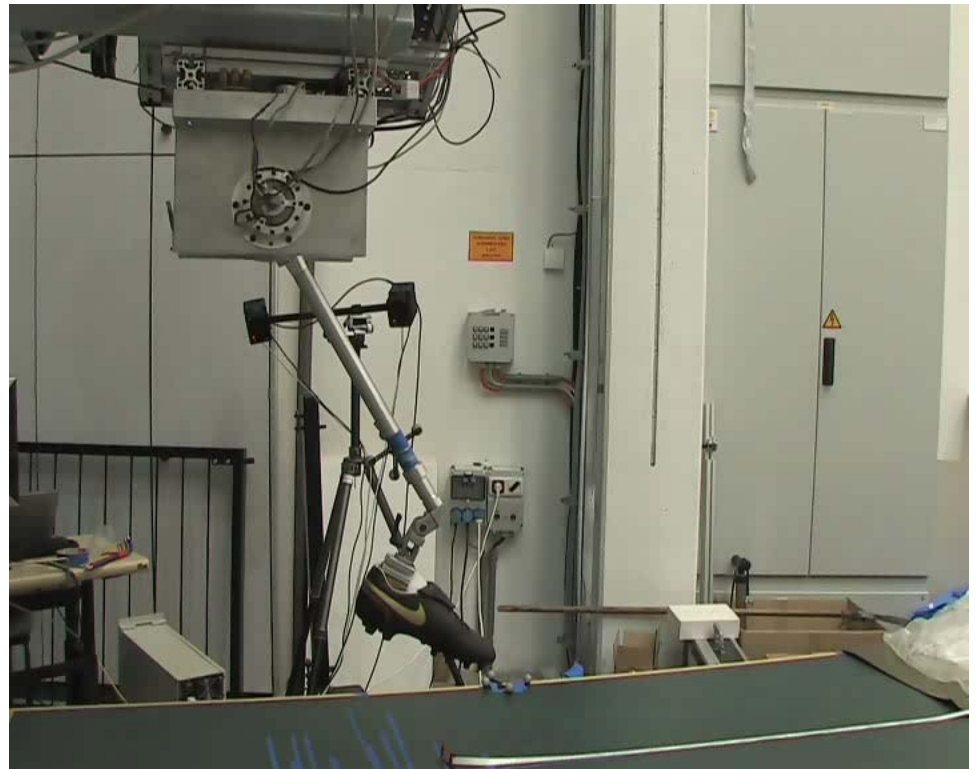
# Active Vibration Damping for VIA Joints

Extension of the passivity based approaches to systems of the form

$$M(q)\ddot{q} + C(q, \dot{q})\dot{q} + \frac{\partial U(q)}{\partial q} = \begin{bmatrix} \tau_m \\ 0 \end{bmatrix}$$



No damping



Active damping

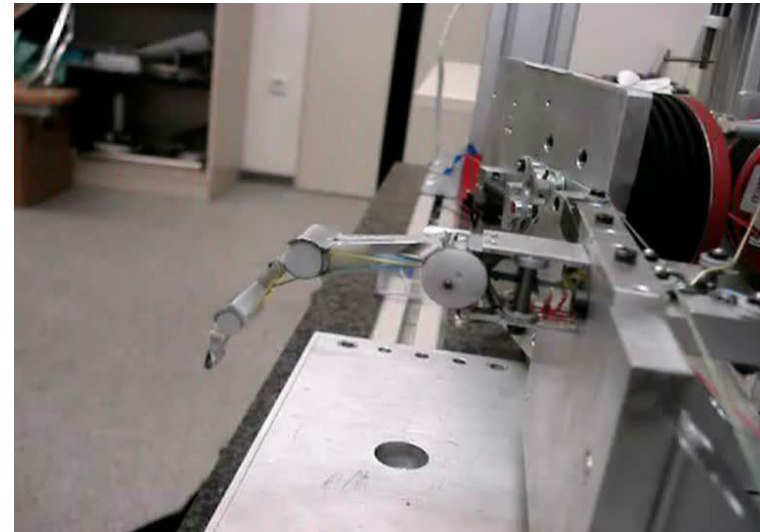
# Performance Validation

Finger:

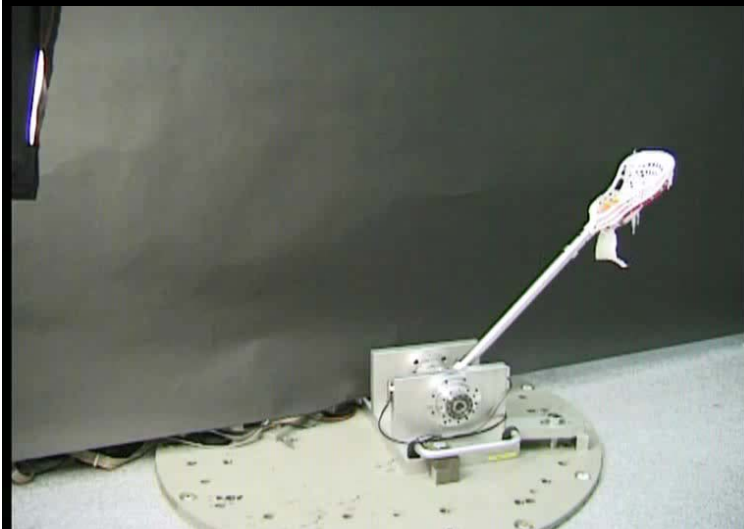
➤ Robust w.r.t. impacts

Arm Joints:

➤ Increase of performance due to energy storage



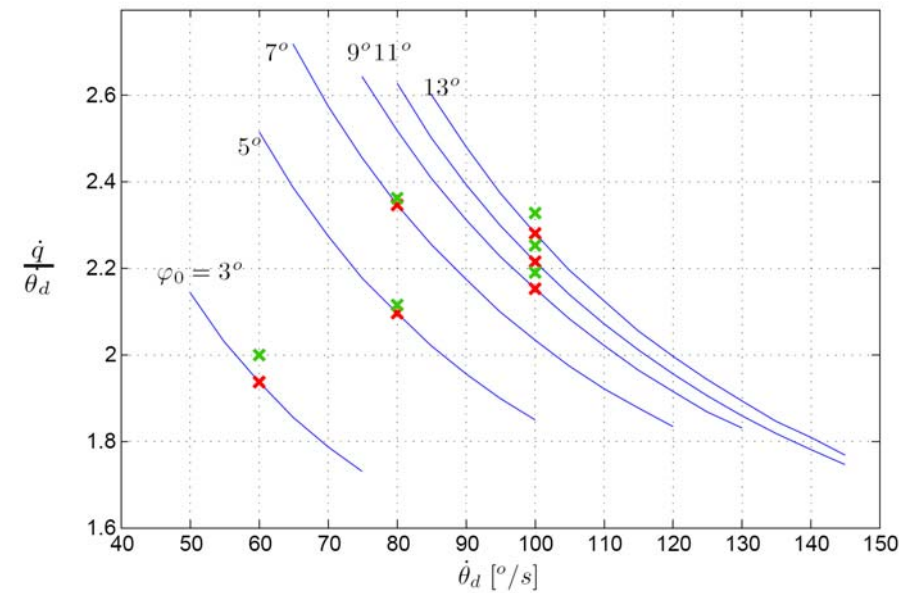
Rigid joint



VIA joint



# Optimal Control for Maximal Performance



Optimized  
stiffness and motion trajectory

# Kicking Performance: Motivation



# Kicking Experiments



DLR

Deutsches Zentrum  
für Luft- und Raumfahrt e.V.  
in der Helmholtz-Gemeinschaft

# Experimental Results

	Stiff Joint	VS-Joint
Speed	3.06 m/s	6.35 m/s
Kicking range	1.6 m	4.05 m
Impact joint torque	85 Nm	10 Nm



# Justin at AUTOMATICA Fair

